Kinematics of shot-geophone migration

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ABSTRACT

In contrast to prestack migration methods based on data binning, common image gathers produced by shot-geophone migration exhibit the appropriate semblance property in either offset domain (focussing at zero offset) or angle domain (focussing at zero slope), when the migration velocity is kinematically correct and when events to be migrated arrive in the data along non-turning rays. The latter condition is required for successful implementation via wavefield depth extrapolation ("survey sinking"). Thus shot-geophone migration may be a particularly appropriate tool for migration velocity analysis of data exhibiting structural complexity.

INTRODUCTION

The basis of migration velocity analysis is the *semblance principle*: prestack migrated data volumes contain *flat image gathers*, i.e. are at least kinematically independent of the bin or stacking parameter, when the velocity is correct (Kleyn, 1983; Yilmaz, 1987). Migration velocity analysis (as opposed to standard NMO-based velocity analysis) is most urgently needed in areas of strong lateral velocity variation, i.e. "complex" structure such as salt flanks, chalk tectonics, and overthrust geology. However strong refraction implies multiple raypaths connecting source and receiver locations with reflection points, and multiple raypaths in turn imply that the semblance principle is not valid: that is, image gathers are *not* in general flat, even when the migration velocity closely approximates the true propagation velocity (Stolk and Symes, 2004).

The failure of the semblance principle in complex structure afflicts all prestack migration techniques based on data binning, i.e. for which each data bin creates an independent

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image. This category includes many variants of common shot, common offset and common scattering angle migration (Nolan and Symes, 1996; Nolan and Symes, 1997; Xu et al., 2001; Brandsberg-Dahl et al., 2003; Stolk, 2002; Stolk and Symes, 2004).

However one well-known form of prestack image formation does not migrate image bins independently: this is Claerbout's survey-sinking migration, or shot-geophone migration (Claerbout, 1971; Claerbout, 1985), commonly implemented using some variety of one-way wave equation to extrapolate source and receiver depths. Such depth extrapolation implementation presumes that rays carrying significant energy travel essentially vertically (dubbed the "DSR condition" by Stolk and De Hoop (2001)). Source and receiver wavefields may be extrapolated separately, and correlated at each depth (shot profile migration), or simultaneously (DSR migration).

This paper demonstrates that a semblance principle appropriate for shot-geophone migration holds regardless of velocity field complexity, assuming

- the DSR condition,
- enough data to determine wavefield kinematics (for example, areal or "true 3D" acquisition in general, or narrow azimuth data plus mild cross-line heterogeneity), and
- a kinematically correct migration velocity field.

This result was established by Stolk and De Hoop (2001). We give a somewhat simpler derivation of this property, and a number of 2D illustrations. This semblance principle takes several roughly equivalent forms, corresponding to several available methods for forming image gathers. Sherwood and Schultz (1982), Claerbout (1985), and others defined image gathers depending on (subsurface) offset and depth: in such offset image gathers, energy is focussed at zero offset when the velocity is kinematically correct. De Bruin et al (1990) and Prucha et al (1999) gave one definition of angle image gathers, while Sava and Fomel (2003) suggest another. Such gathers are functions of scattering angle and depth. In both cases, correct migration velocity focusses energy at zero slope, i.e. angle image gathers are flattened at correct migration velocity.

As a by-product of our analysis, we observe that the semblance principle is a result of the mathematical structure of shot-geophone migration, not of any particular approach to its implementation. In particular, it is not depth extrapolation *per se* that is at the root of if the favorable kinematic properties stated in the last paragraph. Indeed, we show that a shot-geophone variant of two-way reverse time migration (Biondi and Shan, 2002; Symes, 2002) implements the same kinematics hence conforms to the same semblance principle. We even provide a "Kirchhoff" implementation of shot-geophone migration, which also satisfies the semblance principle.

To emphasize the main assertion of this paper: all versions (angle, offset) of the semblance principle for shot-geophone migration hold regardless of degree of multipathing and of computational implementation, provided that the assumptions stated above are valid. In particular, angle imaging via shot-geophone migration, using either method of angle gather formation mentioned above, is *not* equivalent, even kinematically, to surface-oriented common angle imaging (Xu et al., 2001; Brandsberg-Dahl et al., 2003) - indeed, the latter typically generates kinematic artifacts when multiple ray paths carry important energy.

The "enough data" condition listed second above is quite as important as the others, as will be explained below. For arbitrary 3D complexity in the migration velocity field, validity of the semblance principle requires areal coverage ("true 3D" data). In particular we cannot guarantee the absence of kinematic artifacts in shot-geophone migration of narrow azimuth data, unless the velocity model is assumed to have additional properties, for example mild cross-line heterogeneity, which compensate to some extent for the lack of azimuths. This issue will be discussed a bit more in the concluding section.

Sherwood and Schultz (1982) observed that the focusing property of shot-geophone migration might serve as the basis for an approach to velocity estimation. Its freedom from artifacts suggests that shot-geophone migration may be a particularly appropriate tool for migration velocity analysis of data acquired over complex structures. Some preliminary investigations of this idea have been carried out by Shen et al. (2003).

The paper begins with a very general description of shot-geophone migration operator as adjoint to an *extended* Born (single-scattering) modeling operator. All prestack migration methods, including those based on data binning, can be described in this way, as adjoint to extended modeling of some sort. The basic kinematics of shot-geophone prestack migration then follow easily from the high-frequency asymptotics of wave propagation. We summarize these kinematic properties, and present the outline of a complete derivation in appendix A.

When offsets are restricted to be horizontal, as was the case in the original formulation of shot-geophone migration (Claerbout, 1985; Schultz and Sherwood, 1982), and the DSR condition is assumed, the artifact-free result of Stolk and De Hoop (2001) follows easily from the general kinematic properties already described, for both offset image gathers and angle image gathers in the style of Sava and Fomel (2003).

The basic framework does not restrict the subsurface offset vector to be horizontal, nor is one-way wave propagation a necessary part of the formulation. We next introduce the two-way reverse time implementation of horizontal offset shot-geophone migration, both as an interesting algorithm in itself and as a preliminary to the derivation of depth extrapolation migration. Both of the widely used "wave equation" migration families,

shot-profile and double square root migration, follow via replacement of two-way with one-way propagation, as is permitted by the DSR assumption. Double square root migration provides the framework for the alternative construction of angle image gathers due to De Bruin et al. (1990). We show how the semblance property for this form of angle domain migration follows from the general properties of shot-geophone migration.

Finally we present a number of examples illustrating the semblance property, using 2D synthetic data of increasing ray path complexity. Each example contrasts the angle image gathers produced by (Kirchhoff) common scattering angle migration with those produced by shot-geophone migration. In each case, kinematic artifacts appear in the former but not the latter.

SHOT-GEOPHONE MIGRATION AS ADJOINT OF EXTENDED BORN MODELING

We assume that sources and receivers lie on the same depth plane, and adjust the depth axis so that the source-receiver plane is z = 0. This restriction is can be removed at the cost of more complicated notation (and numerics): it is not essential. Nothing about the formulation of the migration method presented below requires that data be given on the full surface z = 0.

While the examples to be presented later are all 2D, the construction is not: in the following \mathbf{x} (and other bold face letters) will denote either two- or three-dimensional vectors. Source locations are \mathbf{x}_s , receiver locations are \mathbf{x}_r .

Single scattering

The causal acoustic Green's function $G(\mathbf{x}, t; \mathbf{x}_s)$ for a point source at $\mathbf{x} = \mathbf{x}_s$ is the solution of

$$\frac{1}{v^2(\mathbf{x})} \frac{\partial^2 G}{\partial t^2}(\mathbf{x}, t; \mathbf{x}_s) - \nabla_{\mathbf{x}}^2 G(\mathbf{x}, t; \mathbf{x}_s) = \delta(\mathbf{x} - \mathbf{x}_s) \delta(t), \tag{1}$$

with G = 0, t < 0.

In common with all other migration methods, shot-geophone migration is based on the Born or single scattering approximation. Denote by $r(\mathbf{x}) = \delta v(\mathbf{x})/v(\mathbf{x})$ a relative perturbation of the velocity field. Linearization of the wave equation yields for the corresponding perturbation of the Green's function

$$\frac{1}{v^2(\mathbf{x})} \frac{\partial^2 \delta G}{\partial t^2}(\mathbf{x}, t; \mathbf{x}_s) - \nabla_{\mathbf{x}}^2 \delta G(\mathbf{x}, t; \mathbf{x}_s) = \frac{2r(\mathbf{x})}{v^2(\mathbf{x})} \frac{\partial^2}{\partial t^2} G(\mathbf{x}, t; \mathbf{x}_s), \tag{2}$$

whose solution has the integral representation at the source and receiver points $\mathbf{x}_r, \mathbf{x}_s$

$$\delta G(\mathbf{x}_r, t; \mathbf{x}_s) = \frac{\partial^2}{\partial t^2} \int d\mathbf{x} \int d\mathbf{r} \frac{2r(\mathbf{x})}{v^2(\mathbf{x})} G(\mathbf{x}, t - \tau; \mathbf{x}_r) G(\mathbf{x}, \tau; \mathbf{x}_s). \tag{3}$$

The singly scattered field is the time convolution of δG with a source wavelet (or the space-time convolution with a radiation pattern operator, for more complex sources). Since the principal concern of this paper is kinematic relationships between data and image, we ignore the filtering by the source signature (i.e. replace it with a delta function). This effective replacement of the source by an impulse does not seem to invalidate the predictions of the theory, though the matter is certainly worthy of more study.

The Born modeling operator F[v] is

$$F[v]r(\mathbf{x}_r, t; \mathbf{x}_s) = \delta G(\mathbf{x}_r, t; \mathbf{x}_s).$$

Common Offset Migration

Basic versions of all prestack migration operators result from two further modeling steps:

- 1. extend the definition of reflectivity to depend on more spatial degrees of freedom, insert somehow into the Born modeling formula (equation (2) or (3)) in such a way that when the extra degrees of freedom are present in some specific way ("physical reflectivity"), Born modeling is recovered;
- 2. form the adjoint of the extended modeling operator: this is a prestack migration operator. The output of the adjoint operator is the prestack image; it depends on the same degrees of freedom as the input of the modeling operator.

Prestack common offset modeling results from replacing $2r(\mathbf{x})/v^2(\mathbf{x})$ with $R(\mathbf{x}, \mathbf{h})$, where \mathbf{h} is vector half-offset: $\mathbf{h} = 0.5(\mathbf{x}_r - \mathbf{x}_s)$. The additional degrees of freedom mentioned in 1. above are the components of source-receiver half-offset. This extended reflectivity is inserted into the Born modeling formula to give the extended common offset modeling operator $\bar{F}[v]$:

$$\bar{F}[v]R(\mathbf{x}_r, t; \mathbf{x}_s) = u(\mathbf{x}_r, t; \mathbf{x}_s),$$

where

$$u(\mathbf{x}_m + \mathbf{h}, t; \mathbf{x}_m - \mathbf{h}) = \frac{\partial^2}{\partial t^2} \int d\mathbf{x} \int d\tau R(\mathbf{x}, \mathbf{h}) G(\mathbf{x}, t - \tau; \mathbf{x}_m + \mathbf{h}) G(\mathbf{x}, \tau; \mathbf{x}_m - \mathbf{h}).$$
(4)

If $R(\mathbf{x}, \mathbf{h}) = 2r(\mathbf{x})/v^2(\mathbf{x})$ is actually independent of \mathbf{h} , then the output $u(\mathbf{x}_r, t; \mathbf{x}_s)$ of equation (4) is identical to the perturbational Green's function $\delta G(\mathbf{x}_r, t; \mathbf{x}_s)$ as is clear from comparing equations (4) and (3). That is, the Born forward modeling operator is the "spray" operator,

$$r(\mathbf{x}) \mapsto R(\mathbf{x}, \mathbf{h}) = 2r(\mathbf{x})/v^2(\mathbf{x}),$$

followed by the common offset forward modeling operator.

The common offset migration operator is the adjoint of this integral operator: its output is the offset-dependent prestack image volume, a function of the same type as the extended common offset reflectivity:

$$\bar{F}^*[v]d(\mathbf{x}, \mathbf{h}) = I_{co}(\mathbf{x}, \mathbf{h}),$$

$$I_{co}(\mathbf{x}, \mathbf{h}) = \int d\mathbf{x}_m \int d\tau \int dt \frac{\partial^2 d}{\partial t^2}(\mathbf{x}_m + \mathbf{h}, t; \mathbf{x}_m - \mathbf{h})G(\mathbf{x}, t - \tau; \mathbf{x}_m + \mathbf{h})G(\mathbf{x}, \tau; \mathbf{x}_m - \mathbf{h}).$$
(5)

Therefore the adjoint of Born modeling (migration, $per\ se$) is common offset migration followed by the adjoint of the "spray" operator: this adjoint is the operator of averaging in \mathbf{h} , i.e. stacking.

Actually the operator defined in equation (5) is only one possible common offset migration operator. Many others follow through application of various weights and filters for example, leaving off the second time derivative in equation (5) amounts to filtering the data before application of $\bar{F}^*[v]$. All of these variations define adjoints to the modeling operator with respect to apppropriate inner products on domain and range spaces. Most important for this investigation, all share a common kinematic description. Therefore we ignore all such variations for the time being, and refer to equation (5) as defining "the" common offset migration operator.

Replacement of the Green's functions in equation (5) by the leading terms in their high frequency asymptotic expansions results in the familiar Kirchhoff common offset migration operator.

Note that both modeling and migration operators share the property that their output for a given **h** depends only on the input for the same value of **h** - that is, they are *block-diagonal* on common offset data bins. This binwise action is responsible for the production of kinematic artifacts when the velocity field refracts rays sufficiently strongly (Stolk and Symes, 2004).

Shot-geophone modeling and migration

Shot-geophone modeling results from a different extension of reflectivity: replace $2r(\mathbf{x})/v^2(\mathbf{x})$ by $R(\mathbf{x}, \mathbf{h})$ where \mathbf{h} is the depth (half)offset mentioned in the introduction. While this extension has exactly the same degrees of freedom as the common offset extended reflectivity, the two are conceptually quite different: \mathbf{h} here has nothing to do with the source-receiver half-offset $0.5(\mathbf{x}_r - \mathbf{x}_s)$!

The shot-geophone modeling operator $\bar{F}[v]$ is given by

$$\bar{F}[v]R(\mathbf{x}_r, t; \mathbf{x}_s) = u(\mathbf{x}_r, t; \mathbf{x}_s),$$

where the field u is defined by

$$u(\mathbf{x}_r, t; \mathbf{x}_s) = \frac{\partial^2}{\partial t^2} \int d\mathbf{x} \int d\mathbf{h} \int d\tau R(\mathbf{x}, \mathbf{h}) G(\mathbf{x} + \mathbf{h}, t - \tau; \mathbf{x}_r) G(\mathbf{x} - \mathbf{h}, \tau; \mathbf{x}_s).$$
 (6)

Note that here \mathbf{x} does play the role of midpoint, though having nothing to do with source-receiver midpoint.

The field $u(\mathbf{x}, t; \mathbf{x}_s)$ is identical to $\delta G(\mathbf{x}, t; \mathbf{x}_s)$ when

$$R(\mathbf{x}, \mathbf{h}) = \frac{2r(\mathbf{x})}{v^2(\mathbf{x})} \delta(\mathbf{h}),$$

i.e. when the generalized reflectivity is concentrated at offset zero. Therefore Born modeling is shot-geophone modeling following the mapping

$$r(\mathbf{x}) \mapsto \frac{2r(\mathbf{x})}{v^2(\mathbf{x})} \delta(\mathbf{h}).$$
 (7)

The shot-geophone migration operator is the adjoint of the shot-geophone modeling operator: it produces an image volume with the same degrees of freedom as the extended shot-geophone reflectivity,

$$\bar{F}^*[v]d(\mathbf{x}, \mathbf{h}) = I_{s-g}(\mathbf{x}, \mathbf{h}),$$

$$I_{s-g}(\mathbf{x}, \mathbf{h}) = \int d\mathbf{x}_r \int d\mathbf{x}_s \int dt \int d\tau \frac{\partial^2 d}{\partial t^2}(\mathbf{x}_r, t; \mathbf{x}_s) G(\mathbf{x} + \mathbf{h}, t - \tau; \mathbf{x}_r) G(\mathbf{x} - \mathbf{h}, \tau; \mathbf{x}_s).$$
(8)

Note that in both equations (6) and (8), all input variables are integrated to produce the value at each output vector: the computation is not block diagonal in **h**, in contrast to the common offset operators defined in equations (4) and (5).

Born migration is shot-geophone migration followed by the adjoint of the mapping defined in equation (7), which is

$$R(\mathbf{x}, \mathbf{h}) \mapsto \frac{2R(\mathbf{x}, 0)}{v^2(\mathbf{x})},$$
 (9)

i.e. shot-geophone migration followed by extraction off the zero offset section.

For some purposes it turns out to be convenient to introduce $sunken\ source\ and\ receiver\ coordinates$

$$\bar{\mathbf{x}}_r = \mathbf{x} + \mathbf{h}, \ \bar{\mathbf{x}}_s = \mathbf{x} - \mathbf{h},$$

and the source-receiver reflectivity \bar{R} by

$$\bar{R}(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s) = R\left(\frac{\bar{\mathbf{x}}_r + \bar{\mathbf{x}}_s}{2}, \frac{\bar{\mathbf{x}}_r - \bar{\mathbf{x}}_s}{2}\right), \text{ i.e. } \bar{R}(\mathbf{x} + \mathbf{h}, \mathbf{x} - \mathbf{h}) = R(\mathbf{x}, \mathbf{h}),$$

and similarly for the image volume I_{s-g} . Change integration variables in equation (8) to get the sunken source-receiver variant of shot-geophone migration:

$$\bar{I}_{s-g}(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s) = \int d\mathbf{x}_r \int d\mathbf{x}_s \int dt \int d\tau \, \frac{\partial^2 d}{\partial t^2}(\mathbf{x}_r, t; \mathbf{x}_s) G(\bar{\mathbf{x}}_r, t - \tau; \mathbf{x}_r) G(\bar{\mathbf{x}}_s, \tau; \mathbf{x}_s).$$

Replacement of the Green's functions in this formula by their high frequency asymptotic (ray-theoretic) approximations results in a Kirchhoff-like representation of shot-geophone migration. See Appendix D for details.

KINEMATICS OF SHOT-GEOPHONE MIGRATION

An event in the data is characterized by its moveout: locally, by a moveout equation $t = T(\mathbf{x}_r, \mathbf{x}_s)$, and infinitesimally by the source and receiver slownesses

$$\mathbf{p}_r = \nabla_{\mathbf{x}_r} T, \ \mathbf{p}_s = \nabla_{\mathbf{x}_s} T$$

Significant energy with this moveout implies that locally near $(\mathbf{x}_r, \mathbf{x}_s, t)$ the data contains a plane wave component with wavenumber $(\omega \mathbf{p}_r, \omega \mathbf{p}_s, \omega)$. These coordinates (position, wavenumber) give the phase space representation of the event.

Note that for incomplete coverage, notably marine streamer geometry, an event in the data will not determine its moveout uniquely. For example, in (idealized) marine streamer geometry, with the streamers oriented along the x axis, the y component of \mathbf{p}_r is not determined by the data. In the discussion to follow, \mathbf{p}_s and \mathbf{p}_r are assumed to be compatible with a data event.

Likewise, a reflector (in the source-receiver representation) at $(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s)$ with wavenumber $(\mathbf{k}_r, \mathbf{k}_s)$ is characterized in (image volume) phase space by these coordinates.

Kinematics with general (3D) offset

The kinematical description of shot-geophone migration relates the phase space coordinates of events and reflectors. An event with phase space representation

$$(\mathbf{x}_r, \mathbf{x}_s, T(\mathbf{x}_r, \mathbf{x}_s), \omega \mathbf{p}_r, \omega \mathbf{p}_s, \omega)$$

is the result of a reflector with (source-receiver) phase space representation $(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s, \mathbf{k}_r, \mathbf{k}_s)$ exactly when

- there is a ray $(\mathbf{X}_s, \mathbf{P}_s)$ leaving the source point $\mathbf{X}_s(0) = \mathbf{x}_s$ at time t = 0 with ray parameter $\mathbf{P}_s(0) = \mathbf{p}_s$, and arriving at $\mathbf{X}_s(t_s) = \bar{\mathbf{x}}_s$ at $t = t_s$ with ray parameter $\mathbf{P}_s(t_s) = -\mathbf{k}_s/\omega$;
- there is a ray $(\mathbf{X}_r, \mathbf{P}_r)$ leaving $\mathbf{X}_r(t_s) = \bar{\mathbf{x}}_r$ at $t = t_s$ with ray parameter $\mathbf{P}_r(t_s) = \mathbf{k}_r/\omega$ and arriving at the receiver point $\mathbf{X}_r(t_r+t_s) = \mathbf{x}_s$ at time $t = T(\mathbf{x}_r, \mathbf{x}_s) = t_r+t_s$ with ray parameter $\mathbf{P}_r(t_r+t_s) = \mathbf{p}_r$.

Figure 1 illustrates this kinematic relation. Appendix A provides a derivation.

Note that since $\mathbf{P}_r, \mathbf{P}_s$ are ray slowness vectors, there is necessarily a length relation between $\mathbf{k}_r, \mathbf{k}_s$: namely,

$$\frac{1}{v(\bar{\mathbf{x}}_r)} = \|\mathbf{P}_r(t_r)\| = \frac{\|\mathbf{k}_r\|}{|\omega|},$$

$$\frac{1}{v(\bar{\mathbf{x}}_s)} = \|\mathbf{P}_s(t_s)\| = \frac{\|\mathbf{k}_s\|}{|\omega|},$$

whence

$$\frac{\|\mathbf{k}_r\|}{\|\mathbf{k}_s\|} = \frac{v(\bar{\mathbf{x}}_s)}{v(\bar{\mathbf{x}}_r)} \tag{10}$$

The kinematics of shot-geophone migration are somewhat strange, so it is reassuring to see that for physical reflectors (i.e. $\bar{R}(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s) = r(\mathbf{x})\delta(\mathbf{h})$) the relation just explained becomes the familiar one of reflection from a reflecting element according to Snell's law. A quick calculation shows that such a physical \bar{R} has a significant local plane wave component near $(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s)$ with wavenumber $(\mathbf{k}_r, \mathbf{k}_s)$ only if $\bar{\mathbf{x}}_r = \bar{\mathbf{x}}_s = \mathbf{x}$ and r has a significant local plane wave component near \mathbf{x} with wavenumber $\mathbf{k}_x = \mathbf{k}_r + \mathbf{k}_s$. From equation (10), \mathbf{k}_r and \mathbf{k}_s have the same length, therefore their sum \mathbf{k}_x is also their bisector, which establishes Snell's law. Thus a single (physical) reflector at \mathbf{x} with wavenumber \mathbf{k}_x gives rise to a reflected event at frequency ω exactly when the rays $(\mathbf{X}_s, \mathbf{P}_s)$ and $(\mathbf{X}_r, \mathbf{P}_r)$ meet at \mathbf{x} at time t_s , and the reflector dip $\mathbf{k}_x = \omega(\mathbf{P}_r(t_s) - \mathbf{P}_s(t_s))$, which is the usual kinematics of single scattering. See Figure 2.

It is now possible to answer the question: in the shot-geophone model, to what extent does a data event determine the corresponding reflector? The rules derived above show that the reflection point $(\bar{\mathbf{x}}_s, \bar{\mathbf{x}}_r)$ must lie on the Cartesian product of two rays, $(\mathbf{X}_s, \mathbf{P}_s)$ and $(\mathbf{X}_r, \mathbf{P}_r)$, consistent with the event, and the total time is also determined. If the coverage is complete, so that the event uniquely determines the source and receiver rays, then the source-receiver representation of the source-receiver reflector must lie along this uniquely determined ray pair. This fact contrasts dramatically with the imaging ambiguities prevalent in all forms of prestack depth migration based on data binning (Nolan and Symes, 1996; Nolan and Symes, 1997; Xu et al., 2001; Prucha et al., 1999; Brandsberg-Dahl et al., 2003; Stolk, 2002; Stolk and Symes, 2004). Even when coverage is complete, in these other forms of prestack migration strong refraction leads to multiple ray pairs connecting data events and reflectors, whence ambiguous imaging of a single event in more than one location within the prestack image volume.

Nonetheless reflector location is still not uniquely determined by shot-geophone migration as defined above, for two reasons:

- Only the total traveltime is specified by the event! Thus if $\bar{\mathbf{x}}_s = \mathbf{X}_s(t_s), \bar{\mathbf{x}}_r = \mathbf{X}_r(t_s)$ are related as described above to the event determining the ray pair, so is $\bar{\mathbf{x}}_s' = \mathbf{X}_s(t_s'), \bar{\mathbf{x}}_r' = \mathbf{X}_r(t_s')$ with $t_s + t_r = t_s' + t_r' = t_{sr}$. See Figure 1.
- Incomplete acquisition, for example limited to a narrow azimuth range as is commonly the case for streamer surveys, may prevent the event from determining its full 3D moveout, as mentioned above. Therefore a family of ray pairs, rather than a unique ray pair, may correspond to the event.

Kinematics with horizontal offset

One way to view the remaining imaging ambiguity in shot-geophone migration as defined so far is to recognize that the image point coordinates $(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s)$ (or (\mathbf{x}, \mathbf{h})) are six-dimensional (in 3D), whereas the data depends on only five coordinates $(\mathbf{x}_r, t, \mathbf{x}_s)$ (at most). Formally, restricting one of the coordinates of the image point to be zero would at least make the variable counts equal, so that unambiguous imaging would at least be conceivable. Since physical reflectivities are concentrated at zero (vector) offset, it is natural to restrict one of the offset coordinates to be zero. The conventional choice, beginning with Claerbout's definition of survey-sinking migration (Claerbout, 1985), is the depth coordinate.

We assume that the shot-geophone reflectivity $R(\mathbf{x}, \mathbf{h})$ takes the form

$$R(\mathbf{x}, \mathbf{h}) = R_z(\mathbf{x}, h_x, h_y)\delta(h_z), \tag{11}$$

leading to the restricted modeling operator:

$$\bar{F}_z[v]R_z(\mathbf{x}_r, t; \mathbf{x}_s) = \frac{\partial^2}{\partial t^2} \int d\mathbf{x} \int dh_x \int dh_y \int d\tau$$

$$R_z(\mathbf{x}, h_x, h_y)G(\mathbf{x} + (h_x, h_y, 0), t - \tau; \mathbf{x}_r)G(\mathbf{x} - (h_x, h_y, 0), \tau; \mathbf{x}_s). \tag{12}$$

The kinematics of this restricted operator follows directly from that of the unrestricted operator, developed in the preceding section.

Denote $\bar{\mathbf{x}}_s = (\bar{x}_s, \bar{y}_s, \bar{z}_s), \mathbf{k}_s = (k_{s,x}, k_{s,y}, k_{s,z})$ etc. For horizontal offset,

$$\bar{R}(\bar{\mathbf{x}}_r, \bar{\mathbf{x}}_s) = \bar{R}_z \left(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \frac{\bar{z}_r + \bar{z}_s}{2} \right) \delta(\bar{z}_r - \bar{z}_s).$$

Fourier transformation shows that \bar{R} has a significant plane wave component with wavenumber $(\mathbf{k}_r, \mathbf{k}_s)$ precisely when \bar{R}_z has a significant plane wave component with wavenumber $k_{r,x}, k_{r,y}, k_{s,x}, k_{s,y}, (k_{r,z} + k_{s,z})$. Thus a ray pair $(\mathbf{X}_r, \mathbf{P}_r), (\mathbf{X}_s, \mathbf{P}_s)$ compatible with a data event with phase space coordinates $(\mathbf{x}_r, \mathbf{x}_s, T(\mathbf{x}_r, \mathbf{x}_s), \omega \mathbf{p}_r, \omega \mathbf{p}_s, \omega)$ images at a point $X_{r,z}(t_s) = X_{s,z}(t_s) = z$, $P_{r,z}(t_s) - P_{s,z}(t_s) = k_z/\omega$, $X_{s,x}(t_s) = x_s$, $P_{s,x}(t_s) = k_{s,x}/\omega$, etc. at image phase space point

$$(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, z, k_{r,x}, k_{s,x}, k_{r,y}, k_{s,y}, k_z).$$

The adjoint of the modeling operator defined in equation (12) is the horizontal offset shot-geophone migration operator:

$$\bar{F}_z^*[v]d(\mathbf{x}, h_x, h_z) = I_{s-g,z}(\mathbf{x}, h_x, h_z),$$

where

$$I_{s-g,z}(\mathbf{x}, h_x, h_z) = \int d\mathbf{x}_r \int d\mathbf{x}_s \int dt \int d\tau$$

$$\frac{\partial^2}{\partial t^2} d(\mathbf{x}_r, t; \mathbf{x}_s) G(\mathbf{x} + (h_x, h_y, 0), t - \tau; \mathbf{x}_r) G(\mathbf{x} - (h_x, h_y, 0), \tau; \mathbf{x}_s)$$
(13)

As mentioned before, operators and their adjoints enjoy the same kinematic relations, so we have already described the kinematics of this migration operator.

Semblance property of horizontal offset image gathers and the DSR condition

As explained by Stolk and De Hoop (2001), Claerbout's survey sinking migration is kinematically equivalent to shot-geophone migration as defined here, under two assumptions:

- subsurface offsets are restricted to horizontal $(h_z = 0)$;
- rays (either source or receiver) carrying significant energy are nowhere horizontal, i.e. $P_{s,z} > 0$, $P_{r,z} < 0$ throughout the propagation;
- events in the data determine full (four-dimensional) slowness P_r, P_s .

We call the second condition the "Double Square Root", or "DSR", condition, for reasons explained by Stolk and De Hoop (2001). This reference also offers a proof of the **Claim:** Under these restrictions, the imaging operator \bar{F}_z^* can image a ray pair at precisely one location in image volume phase space. When the velocity is correct, the image energy is therefore concentrated at zero offset in the image volume $I_{s-g,z}$.

The demonstration presented by Stolk and De Hoop (2001) uses oscillatory integral representations of the operator \bar{F}_z and its adjoint. However, the conclusion also follows directly from the kinematic analysis above and the DSR condition.

Indeed, note that the DSR condition implies that depth is increasing along the source ray, and decreasing along the receiver ray - otherwise put, depth is increasing along both rays, if you traverse the receiver ray backwards. Therefore depth can be used to parametrize the rays. With depth as the parameter, time is increasing from zero along the source ray, and decreasing from t_{sr} along the receiver ray (traversed backwards). Thus the two times can be equal (to t_s) at exactly one point.

Since the scattering time t_s is uniquely determined, so are all the other phase space coordinates of the rays. If the ray pair is the incident-reflected ray pair of a reflector, then the reflector must be the *only* point at which the rays cross, since there is only one time t_s at which $X_{s,z}(t_s) = X_{r,z}(t_s)$. See Figure 3. Therefore in the infinite frequency limit the energy of this incident-reflected ray pair is imaged at zero offset, consistent with Claerbout's imaging condition.

If furthermore coverage is complete, whence the data event uniquely determines the full slowness vectors, hence the rays, then it follows that a data event is imaged at precisely one location, namely the reflector which caused it, and in particular focusses at zero offset. This is the offset version of the result established by Stolk and De Hoop (2001), for which we have now given a different (and more elementary) proof.

Remark: Note that the DSR assumption precludes the imaging or near- or post-vertical reflectors, since in general for such reflectors it will not be possible to satisfy the imaging conditions without either incident or reflected ray turning horizontal at some point.

Semblance property of angle image gathers via Radon transform in offset and depth

According to Sava and Fomel (2003), angle image gathers A_z may be defined via Radon transform in offset and depth of the offset image gathers constructed above, i.e. the migrated data volume $I_{s-g,z}(\mathbf{x}, h_x, h_y)$ (defined in equation (13)) for fixed x, y:

$$A_z(x, y, \zeta, p_x, p_y) = \int dh_x \int dh_y I_{s-g,z}(x, y, \zeta + p_x h_x + p_y h_y, h_x, h_y),$$

in which ζ denotes the z-intercept parameter, and p_x and p_y are the x and y components of offset ray parameter. The ray parameter components may then be converted to angle (Sava and Fomel, 2003). As is obvious from this formula, if the energy in $I_{s-g,z}(\mathbf{x}, h_x, h_y)$ is focussed, i.e. localized, on $h_x = 0, h_y = 0$, then the Radon transform A_z will be (essentially) independent of p_x, p_y . That is, when displayed for fixed x, y with ζ axis plotted vertically and p_x and p_y horizontally, the events in A_z will appear flat. The converse is also true. This is the semblance principle for angle gathers.

WAVE EQUATION MIGRATION

The DSR assumption and the horizontal offset restriction (equation (11)) are assumed to hold throughout the following discussion.

The preceding sections defined shot-geophone modeling operators and their dual migration operators via integral representation, using the acoustic Green's function. In this section we derive several alternate definitions of these operators based on the solution of boundary value problems for one- and two-way wave equations. These definitions are the basis of efficient computational migration algorithms. We show that the imaging operators defined by solving these problems differ from the shot-geophone migration operator only by filters and amplitude factors which do not alter kinematic relations. Therefore these operators inherit the semblance properties of shot-geophone migration established in the last section. We also establish a similar semblance property for a second definition of angle image gathers.

Two-way reverse time migration

Migration algorithms based on reverse time wave propagation date back to Whitmore (1983). The extension to shot-geophone migration appears to be more recent (Biondi and Shan, 2002; Symes, 2002).

The derivation of reverse time shot-geophone migration begins with the source-receiver coordinate rewrite of equation (12),

$$\bar{F}_z[v]\bar{R}_z(\mathbf{x}_r, t; \mathbf{x}_s) = \frac{\partial^2}{\partial t^2} \int d\bar{x}_r \int d\bar{y}_r \int d\bar{x}_s \int d\bar{y}_s \int d\tau$$

$$\bar{R}_z\left(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \frac{\bar{z}_r + \bar{z}_s}{2}\right) \delta(\bar{z}_r - \bar{z}_s) G(\mathbf{x}_r, t - \tau; \bar{\mathbf{x}}_r) G(\bar{\mathbf{x}}_s, \tau; \mathbf{x}_s). \tag{14}$$

The defining property of the acoustic Green's function shows that

$$\bar{F}_z[v]\bar{R}_z(\mathbf{x}_r, t; \mathbf{x}_s) = u(\mathbf{x}_r, t; \mathbf{x}_s),$$

where u solves the inhomogeneous wave equation

$$\left(\frac{1}{v^2(\bar{\mathbf{x}}_r)}\frac{\partial^2}{\partial t^2} - \nabla_{\bar{\mathbf{x}}_r}^2\right) u(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) = w_s(\bar{\mathbf{x}}_r, t; \mathbf{x}_s), \tag{15}$$

and

$$w_s(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) = \int d\bar{x}_s \int d\bar{y}_s \bar{R}_z \left(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \frac{\bar{z}_r + \bar{z}_s}{2}\right) \delta(\bar{z}_r - \bar{z}_s) \frac{\partial^2}{\partial t^2} G(\bar{\mathbf{x}}_s, t; \mathbf{x}_s). \tag{16}$$

Equation (15) is the shot-geophone analogue of the Born forward modeling equation (2). A standard trick, the so-called *adjoint state method*, computes the output (image volume) $I_{s-g,z}$ of the adjoint operator $\bar{F}_z[v]^*$, applied to the data:

$$I_{s-g,z}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}) = \bar{F}_z[v]^* d(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z})$$

$$= \int d\mathbf{x}_s \int dt u^*(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) \frac{\partial^2 G}{\partial t^2}(\bar{\mathbf{x}}_s, t; \mathbf{x}_s) \bigg|_{\bar{z}_r = \bar{z}_s = \bar{z}}.$$
(17)

The adjoint state field u^* solves

$$\left(\frac{1}{v(\bar{\mathbf{x}}_r)^2}\frac{\partial^2}{\partial t^2} - \nabla_{\bar{\mathbf{x}}_r}^2\right)u^*(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) = \int d\mathbf{x}_r d(\mathbf{x}_r, t; \mathbf{x}_s)\delta(\mathbf{x}_r - \bar{\mathbf{x}}_r), \tag{18}$$

and $u^* \equiv 0, t >> 0, z > 0$. The adjoint state equation (18) backpropagates the timereversed data, so the adjoint state field u^* is sometimes known as the "receiver wave field". It is important to note that the field u^* is not the physical reflected field u, timereversed - it is simply a convenient mathematical artifact which plays a key role in an efficient computation of the adjoint operator $\bar{F}_z[v]^*$. A reverse time shot-geophone migration algorithm is a computational implementation of the equations (17), (18).

For future reference, note that the reciprocity principle for acoustic Green's functions (Aki and Richards (1980), pp. 24-28) implies that the right hand side of equation (16) is itself the solution of an inhomogeneous wave equation, with the source location playing the role of spatial coordinate:

$$\left(\frac{1}{v^2(\bar{\mathbf{x}}_s)}\frac{\partial^2}{\partial t^2} - \nabla_{\bar{\mathbf{x}}_s}^2\right) w_s(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) = q(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s), \tag{19}$$

in which

$$q(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) = \bar{R}_z \left(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \frac{\bar{z}_r + \bar{z}_s}{2} \right) \delta(\bar{z}_r - \bar{z}_s) \frac{\partial^2}{\partial t^2} \delta(t).$$

One can view equation (19) as propagating the "source wave field" (i.e. w_s). In the construction of the image volume (equation (17)) requires only the values of the field $w(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s)$ at the actual source points $\bar{\mathbf{x}}_s = \mathbf{x}_s$.

Again by reciprocity, one can reverse the roles of source and receiver coordinates throughout the above derivation. Thus u also solves

$$\left(\frac{1}{v^2(\bar{\mathbf{x}}_s)}\frac{\partial^2}{\partial t^2} - \nabla_{\bar{\mathbf{x}}_s}^2\right) u(\mathbf{x}_r, t; \bar{\mathbf{x}}_s) = w_r(\mathbf{x}_r, t; \bar{\mathbf{x}}_s).$$
(20)

The field w_r is a solution of its own wave equation, analogously to w_s :

$$\left(\frac{1}{v^2(\bar{\mathbf{x}}_r)}\frac{\partial^2}{\partial t^2} - \nabla_{\bar{\mathbf{x}}_r}^2\right) w_r(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) = q(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s).$$
(21)

It is important to note that the right-hand sides of the equations (19), (21) are the same.

One-way wave propagation

A solution of the inhomogeneous wave equation

$$\left(\frac{1}{v^2(\mathbf{x})}\frac{\partial^2}{\partial t^2} - \nabla_{\mathbf{x}}^2\right)u(\mathbf{x}, t) = f(\mathbf{x}, t)$$
(22)

is upgoing if its high frequency components propagate along rays along which depth decreases with increasing time. Such wavefields also satisfy a one-way wave equation, an evolution equation in decreasing z:

$$\frac{\partial u}{\partial z}(\mathbf{x}, t) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\mathbf{x})\frac{\partial^2}{\partial t^2} + \nabla_{x,y}^2}\right)u(\mathbf{x}, t) + (C_-u)(\mathbf{x}, t) + (A_-f)(\mathbf{x}, t). \tag{23}$$

See (Stolk, 2004) and references cited there for detailed derivations.

Downgoing wavefields solve a similar equation with a plus sign on the RHS.

It is also necessary to impose an initial condition at either large positive or large negative z, as equation (23) defines an evolution in z. If the solution is required to vanish for large positive z, then it carries energy upwards and forward in time. Vanishing for large negative z implies energy transport downwards and backward in time.

The approximation sign in equation (23) is present because the two sides differ by a smoother error, lower in frequency content than the terms displayed, like the error in a ray-theoretic approximation.

For various reasons, the square root operator $-\mathrm{i}\sqrt{-v^{-2}(\mathbf{x})\frac{\partial^2}{\partial t^2}+\nabla_{x,y}^2}$ can only be defined approximately. The square root operator and the operators A_- and C_- appearing in the one-way equation (23) for the two-way solution are quite special in that they do not modify the location or orientation of high-frequency components of the functions to which they are applied. These operators are a combination of (stationary) filters and amplitude factors. The precise nature of the square root operator and the operators A_- and C_- is discussed a bit further in Appendix C.

The square root operator is real, i.e. a real input function results in a real output function. The same is true of the operators C_{\pm} , A_{\pm} . This somewhat non-obvious assertion is justified in Appendix C. The main consequence of reality is that with real data (value of u for fixed z, right hand side f), the solution of the evolution problem (23) is real a comforting conclusion, as these fields are supposed to represent physical time-domain quantities. The square root operator is also skew-adjoint, i.e. its adjoint is its negative.

Computationally efficient approximation of the square root operator is the subject of a large literature, especially for the case of laterally varying velocity fields v - see (Le Rousseau and De Hoop, 2001) for a variant of one approach and many references. In particular, computationally useful approximations must suppress wavefield components with near-horizontal ray velocities (near-evanescent waves), both order to keep the extrapolation stable and to avoid gross phase inaccuracy. Thus only part of the one-way wavefield is computed in practice.

In the remainder of this section we will derive two major families of widely used migration algorithms by simply replacing the wave equation by its one-way analogue, i.e. dropping the operators C_{\pm} , A_{\pm} from equation (23) and related equations. This simplification is possible if one demands only that migration reproduce the *structure* of the shot-geophone reflectivity \bar{R}_z , i.e. the locations and orientations of its high frequency components. Migration and modeling operators are adjoint to each other, and share the same reflector - to - reflection - event relation. Therefore any modification of the modeling equations that preserves this relation also preserves the critical imaging property of the corresponding migration.

We will use several times the following two observations:

i. Assuming that u is an upgoing solution of the inhomogeneous wave equation (22), the solution \tilde{u} of

$$\frac{\partial \tilde{u}}{\partial z}(\mathbf{x}, t) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\mathbf{x})\frac{\partial^2}{\partial t^2} + \nabla_{x,y}^2}\right) \tilde{u}(\mathbf{x}, t) + f(\mathbf{x}, t). \tag{24}$$

has high frequency components in the same locations in space-time and with the same orientations as does u.

ii. if f and \tilde{f} share locations and orientations of high frequency components, then the locations and orientations of high frequency components of the solution \tilde{u} of (24) does not change if f is replaced by \tilde{f} .

Appendix C gives a sketch of the asymptotic analysis leading to these observations.

Note that if one demands more than structural fidelity of migration, then the operators appearing in equation (23) must be taken more seriously. For example, so-called true amplitude migration algorithms based on one-way propagation involve approximations to the operators C_{\pm} and A_{\pm} in addition to approximation of the square root operator. See Stolk (2004) for a detailed treatment of this point.

Shot profile migration

The DSR hypothesis implies that the wavefields appearing in reverse time migration (17) are downgoing (G) or upgoing (u^*) . Claerbout (Claerbout, 1971) suggested that these may be expressed as solutions of one-way equations, and identified the appropriate imaging condition. From equation (23),

$$\frac{\partial u^*}{\partial \bar{z}_r}(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r)}\frac{\partial^2}{\partial t^2} + \nabla^2_{\bar{x}_r, \bar{y}_r}\right) u^*(\bar{\mathbf{x}}_r, t; \mathbf{x}_s)
+ (C_-u^*)(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) + (A_-d_s)(\bar{\mathbf{x}}_r, t; \mathbf{x}_s), \ u^* \equiv 0, \ \bar{z}_r < 0
d_s(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) = \int dx_r d(\mathbf{x}_r, t; \mathbf{x}_s)\delta(\bar{\mathbf{x}}_r - \mathbf{x}_r)
\frac{\partial G}{\partial \bar{z}_s}(\bar{\mathbf{x}}_s, t; \mathbf{x}_s) \simeq \mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_s)}\frac{\partial^2}{\partial t^2} + \nabla^2_{\bar{x}_s, \bar{y}_s}\right) G(\bar{\mathbf{x}}_s, t; \mathbf{x}_s)
+ (C_+G)(\bar{\mathbf{x}}_s, t; \mathbf{x}_s) + (A_+e_s)(\bar{\mathbf{x}}_s, t; \mathbf{x}_s), \ G \equiv 0, \ \bar{z}_s < 0
e_s(\bar{\mathbf{x}}_s, t; \mathbf{x}_s) = \delta(\bar{\mathbf{x}}_s - \mathbf{x}_s)\delta(t)$$
(25)

Note that only the downgoing part of the acoustic Green's function is produced by solving the initial value problem (26) - but this is fine, as all heterogeneity in the earth is assumed to lie in z > 0!

In view of the remarks at the end of the last section, we replace u^* and G by the solutions R and S of the simplified one-way equations

$$\frac{\partial R}{\partial \bar{z}_r}(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r)}\frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_r, \bar{y}_r}^2\right) R(\bar{\mathbf{x}}_r, t : \mathbf{x}_s)
+ d_s(\bar{\mathbf{x}}_r, t; \mathbf{x}_s), \quad R \equiv 0, \quad \bar{z}_r < 0
\frac{\partial S}{\partial \bar{z}_s}(\bar{\mathbf{x}}_s, t; \mathbf{x}_s) \simeq \mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_s)}\frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_s, \bar{y}_s}^2\right) S(\bar{\mathbf{x}}_s, t : \mathbf{x}_s)
+ e_s(\bar{\mathbf{x}}_s, t; \mathbf{x}_s), \quad R \equiv 0, \quad \bar{z}_s < 0$$
(28)

The "downward continued source field" S and the "downward continued receiver field" R have the same high frequency geometry as do the adjoint field u^* and the Green's function G respectively. Therefore the cross-correlation at zero time lag

$$I_{SR}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}) = \int dx_s \int dt R(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) S(\bar{\mathbf{x}}_s, t; \mathbf{x}_s) \bigg|_{\bar{z}_r = \bar{z}_s = \bar{z}}$$
(29)

has the same high-frequency components, i.e. exposes the same *structure*, as does the output of the migration operator $\bar{F}_z[v]^*$ represented by equation (17). This is the imaging condition identified by Claerbout (1971).

A shot profile migration algorithm, i.e. computational implementation of equations (27), (28), and (29), typically takes the form of an accumulation loop for (29) over shot position \mathbf{x}_s , as both (27) and (28) are solvable independently for each \mathbf{x}_s .

In practice, the inhomogeneous evolution problem (27) is replaced by the homogeneous problem with inhomogeneous initial conditions,

$$\frac{\partial R}{\partial \bar{z}_r}(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r)\frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_r, \bar{y}_r}^2}\right) R(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) = 0,$$

$$R(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s)|_{\bar{z}_r = 0} = d(\bar{\mathbf{x}}_r, t; \mathbf{x}_s).$$
(30)

In view of Duhamel's principle, the solutions of equations (27), (30) are exactly the same for $\bar{z}_r > 0$. A similar modification is usually made to the problem (28).

Double-square-root migration

The DSR hypothesis implies that the acoustic wavefield u appearing in the shotgeophone forward modeling equation (15) is upgoing. Therefore u also satisfies the oneway wave equation

$$\frac{\partial u}{\partial \bar{z}_r}(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r)\frac{\partial^2}{\partial t^2} + \nabla^2_{\bar{x}_r, \bar{y}_r}}\right) u(\bar{\mathbf{x}}_r, t: \bar{\mathbf{x}}_s)$$

$$+(C_{-,r}u)(\bar{\mathbf{x}}_r,t;\bar{\mathbf{x}}_s) + (A_{-,r}w_s)(\bar{\mathbf{x}}_r,t;\bar{\mathbf{x}}_s). \tag{31}$$

The additional subscript on the operators A_-, C_- indicates that they act on the $\bar{\mathbf{x}}_r, t$ variables.

Since the wavefield w_s defined by equation (16) is required only for $\bar{\mathbf{x}}_s \sim \mathbf{x}_s$, i.e. for $\bar{z}_s > \bar{z}_r$, DSR also implies that w_s is an upgoing solution of its wave equation, whence

$$\frac{\partial w_s}{\partial \bar{z}_s}(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_s)}\frac{\partial^2}{\partial t^2} + \nabla^2_{\bar{x}_s, \bar{y}_s}\right) w_s(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) + (C_{-,s}w_s)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) + (A_{-,s}q)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \tag{32}$$

with $w_s \equiv 0$ for large \bar{z}_s .

The DSR assumption also implies one-way versions of equations (20) and (19):

$$\frac{\partial u}{\partial \bar{z}_s}(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_s)}\frac{\partial^2}{\partial t^2} + \nabla^2_{\bar{x}_s, \bar{y}_s}\right) u(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s)
+ (C_{-,s}u)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) + (A_{-,s}w_r)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s).$$

$$\frac{\partial w_r}{\partial \bar{z}_r}(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \simeq -\mathrm{i}\left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r)}\frac{\partial^2}{\partial t^2} + \nabla^2_{\bar{x}_r, \bar{y}_r}\right) w_r(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s)
+ (C_{-,r}w_r)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) + (A_{-,r}q)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s)$$
(34)

and $w_r \equiv 0$ for large \bar{z}_r .

Equations (31)-(34) imply a dynamical law for the horizontal offset wavefield

$$\bar{u}_{\mathrm{DSR}}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t) \equiv u(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s)|_{\bar{z}_r = \bar{z}_s = \bar{z}}$$

namely

$$\frac{\partial}{\partial \bar{z}} \bar{u}_{\text{DSR}}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t) = \frac{\partial u}{\partial \bar{z}_r}(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \Big|_{\bar{z}_r = \bar{z}_s = \bar{z}} + \frac{\partial u}{\partial \bar{z}_s}(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \Big|_{\bar{z}_r = \bar{z}_s = \bar{z}}$$

$$\simeq -i \left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_r, \bar{y}_r}^2} + \sqrt{-v^{-2}(\bar{\mathbf{x}}_s) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_s, \bar{y}_s}^2} \right) \bar{u}_{\text{DSR}}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t) \quad (35)$$

$$+ \left[((C_{-,r} + C_{-,s})u)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) + (A_{-,r}w_s)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) + (A_{-,s}w_r)(\bar{\mathbf{x}}_r, t; \bar{\mathbf{x}}_s) \right]_{\bar{z}_r = \bar{z}_s = \bar{z}}.$$

This equation can be simplified by systematic use of the observations (i) and (ii) on the relation between acoustic and one-way fields. Note that the second time derivative can be dropped from the definition of q, without altering the geometry of the high frequency wavefields.

With these modifications, equations (32), (34) are ordinary differential equations in \bar{z}_r , \bar{z}_s respectively (with operator coefficients), with a factor of $\delta(\bar{z}_r - \bar{z}_s)$ in each right hand side. Further, the fields w_r, w_s vanish for $\bar{z}_r > \bar{z}_s$, $\bar{z}_s > \bar{z}_r$ respectively. It is easy to see that the solution to such a problem has a jump at the location of the delta function, of magnitude equal to the coefficient of $\delta(\bar{z}_r - \bar{z}_s)$. Therefore the sum of the values of w_r, w_s at $\bar{z}_r = \bar{z}_s = \bar{z}$ appearing in equation (35) is exactly $2\bar{R}_z$. For our final modification not changing any of the structural relations, drop the factor of 2.

Denote what has become of \bar{u}_{DSR} after all of these changes by u_{DSR} . We have shown that u_{DSR}

- i. has the same positions and orientations of high-frequency components as does $\bar{u}_{\rm DSR}$, hence expresses the same reflector to reflection event relationship, and
- ii. solves the double square root modeling equation

$$\frac{\partial}{\partial \bar{z}} u_{\text{DSR}}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t)$$

$$\simeq -i \left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_r, \bar{y}_r}^2} + \sqrt{-v^{-2}(\bar{\mathbf{x}}_s) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_s, \bar{y}_s}^2} \right) u_{\text{DSR}}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t) \quad (36)$$

$$+ \bar{R}_z(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}) \delta(t)$$

The double square root modeling operator $\bar{F}_{DSR}[v]$ maps \bar{R}_z to the values of the field u_{DSR} at the source/receiver locations (and z=0):

$$\bar{F}_{DSR}[v]\bar{R}_z(x_r, x_s, y_r, y_s, t) = u_{DSR}(x_r, x_s, y_r, y_s, 0, t).$$

Note that the modeling operator factors: $\bar{F}_{DSR}[v] = HT$, where T is the time injection operator

$$(T\bar{R}_z)(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t) = \bar{R}_z(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z})\delta(t),$$

and H is the solution operator of the double square root wave equation: for a source field $f(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t)$,

$$Hf(x_r, x_s, y_r, y_s, t) = u(x_r, x_s, y_r, y_s, 0, t)$$

where

$$\frac{\partial}{\partial \bar{z}} u(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t)$$

$$\simeq -i \left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r)} \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_r, \bar{y}_r}^2 + \sqrt{-v^{-2}(\bar{\mathbf{x}}_s)} \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_s, \bar{y}_s}^2 \right) u(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t)$$

$$+ f(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t)$$
(37)

and $u \equiv 0, \bar{z} >> 0$ (i.e. initial value problem in decreasing \bar{z}).

The double square root migration operator $\bar{F}_{DSR}[v]^*$, adjoint to the modeling operator, also factors:

$$\bar{F}_{DSR}[v]^* = T^*H^*.$$
 (38)

The adjoint of the time injection operator T^* is easily seen to be restriction to t = 0. The adjoint of the double square root solution operator H^* , applied to data d, turns out to be the solution of the initial value problem in *increasing* \bar{z} :

$$\frac{\partial}{\partial \bar{z}} u_{\text{DSR}}^*(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t)$$

$$\simeq -i \left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_r, \bar{y}_r}^2} + \sqrt{-v^{-2}(\bar{\mathbf{x}}_s) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_s, \bar{y}_s}^2} \right) u_{\text{DSR}}^*(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t),$$

$$u_{\text{DSR}}^*(x_r, x_s, y_r, y_s, 0, t) = d(x_r, x_s, y_r, y_s, t)$$
(39)

[This representation is another application of the adjoint state idea, and is explained in Appendix B.]

Thus the factorization (38) reveals the usual description of double square root migration (Claerbout, 1985):

- simultaneously downward continue sources and receivers $(d \mapsto H^*d)$;
- extract t = 0 section I_{DSR} ($H^*d \mapsto T^*H^*d = I_{DSR}$).

Explicitly, the DSR image volume $I_{DSR} = \bar{F}_{DSR}[v]d$ is defined by

$$I_{\text{DSR}}(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}) = u_{\text{DSR}}^*(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, 0)$$
(40)

Semblance property of angle gathers via Radon transform in offset and time

Denote by D the downward continued data field u_{DSR}^* , expressed in midpoint-offset coordinates:

$$D(\mathbf{x}, h_x, h_y, t) \equiv u_{\text{DSR}}^*(x + h_x, x - h_x, y + h_y, y - h_y, z, t)$$

Angle gathers obtained via Radon transform in offset and time of $D(\mathbf{x}, h_x, h_y, t)$ were introduced by (de Bruin et al., 1990), and discussed further in (Prucha et al., 1999). We denote these gathers by

$$B_z(\mathbf{x}, p_x, p_y) = \int dh_x \int dh_y D(\mathbf{x}, h_x, h_y, p_x h_x + p_y h_y). \tag{41}$$

The purpose of this section is to establish the semblance property of the angle gathers B_z .

Note that the Radon transform in definition (41) is evaluated at zero (time) intercept. The dependence on z is carried by the coordinate plane in which the Radon transform is performed, rather than by the (z-) intercept as was the case with the Sava-Fomel angle gathers A_z defined previously. Also note that B_z requires the double square root field D (or u^*), whereas A_z may be constructed with the image output by any version of shot-geophone migration.

We first need to establish at which points $(\mathbf{x}, h_x, h_y, t)$ significant energy of D is located. The argument for \bar{D} is slightly different from the argument for \bar{I}_z , since \bar{D} depends also on the time. For \bar{I}_z there was a kinematic relation $(\mathbf{x}_s, \mathbf{x}_r, t_{sr}, \omega \mathbf{p}_s, \omega \mathbf{p}_r, \omega)$ to a point in phase space $(x_s, x_r, y_s, y_r, z, k_{s,x}, k_{r,x}, k_{s,y}, k_{r,y}, k_z)$ where the energy in \bar{I}_z is located. The restriction of \bar{D} to time τ is the same as the restriction to time 0, but using time-shifted data $d(..., t-\tau)$. Therefore we can follow almost the same argument as for the kinematic relation of \bar{I}_z . We find that for an event at $(\mathbf{x}_s, \mathbf{x}_r, t_{sr}, \omega \mathbf{p}_s, \omega \mathbf{p}_r, \omega)$ to contribute at \bar{D} , restricted to time τ , we must have that (x_s, y_s, z) is on the ray \mathbf{X}_s , say at time (t'_s) , i.e. $(x_s, y_s, z) = \mathbf{X}_s(t'_s)$. Then (x_r, y_r, z) must be on the ray \mathbf{X}_r say at time t''_s , i.e. $(x_r, y_r, z) = \mathbf{X}_r(t''_s)$. The situation is displayed in Figure 4, using midpoint-offset coordinates. Furthermore, the sum of the traveltimes from \mathbf{x}_s to (x_s, y_s, z) and from \mathbf{x}_r to (x_r, y_r, z) must be equal to $t_{sr} - \tau$. It follows that $t''_s - t'_s = \tau$.

Now consider an event from a physical reflection at $\mathbf{X}_s(t_s) = \mathbf{X}_r(t_s) = (x_{\text{scat}}, y_{\text{scat}}, z_{\text{scat}})$. We use the previous reasoning to find where the energy in D is located (in midpoint-offset coordinates). We will denote by $(v_{s,x}(t), v_{s,y}(t), v_{s,z}(t))$ the ray velocity for the source ray $\frac{d\mathbf{X}_s}{dt}$. The horizontal "sunken source" coordinates $(x - h_x, y - h_y)$ then satisfy

$$x_{\text{scat}} - (x - h_x) = \int_{t_s'}^{t_s} dt \, v_{s,x}(t), \quad y_{\text{scat}} - (y - h_y) = \int_{t_s'}^{t_s} dt \, v_{s,y}(t), \tag{42}$$

For the "sunken receiver" coordinates we find

$$(x + h_x) - x_{\text{scat}} = \int_{t_s}^{t_s''} dt \, v_{r,x}(t), \quad (y + h_y) - y_{\text{scat}} = \int_{t_s}^{t_s''} dt \, v_{r,y}(t). \tag{43}$$

Adding up the x components of these equations, and separately the y components of these equations gives that

$$2h_x = \int_{t_s'}^{t_s''} v_x(t)dt, \quad 2h_y = \int_{t_s'}^{t_s''} v_y(t)dt,$$

where now the velocity (v_x, v_y) is from the source ray for $t < t_s$, and from the receiver ray for $t > t_s$. Let us denote by $v_{\parallel,\text{max}}$ the maximal horizontal velocity along the rays between $(x_{\text{scat}}, y_{\text{scat}}, z_{\text{scat}})$ and the points (x_s, y_s, z) and (x_r, y_r, z) , then we have

$$2\|(h_x, h_y)\| \le |t_s'' - t_s'|v_{\parallel, \max} = |\tau|v_{\parallel, \max}. \tag{44}$$

When we plot the locations of the energy in \bar{D} in the $(\|(h_x, h_y)\|, \tau)$ plane, we find the shaded region in Figure 5.

The angle transform in equation (41) is an integral of D over a plane in the (h_x, h_y, τ) volume given by

$$\tau = p_x h_x + p_y h_y.$$

Suppose now that

$$\sqrt{p_x^2 + p_y^2} < \frac{2}{v_{\parallel,\text{max}}},\tag{45}$$

Then we have

$$|\tau| = |p_x h_x + p_y h_y| < \frac{2}{v_{\parallel,\text{max}}} \|(h_x, h_y)\|.$$

In other words the planes of integration are not in the shaded region of the $(\|(h_x, h_y)\|, \tau)$ plane. The only points where these planes of integration intersect the set of (h_x, h_y, t) where energy of D is located, are points with $\tau = 0, h_x = h_y = 0$. It follows that the energy in the angle transform of equation (41) is located only at the true scattering point independent of (p_x, p_y) . We conclude that the semblance property also holds for the angle transform via Radon transform in the offset time domain, provided that (45) holds.

The bound $v_{\parallel,\text{max}}$ need not be a global bound on the horizontal component of the ray velocity. The integral in equation (41) is over some finite range of offsets, hence on some finite range of times, so that the distance between say the midpoint \mathbf{x} in equation (41), and the physical scattering point is bounded. Therefore $v_{\parallel,\text{max}}$ should be a bound on the horizontal component of the ray velocity on some sufficiently large region around \mathbf{x} .

EXAMPLES

In three 2D synthetic data examples we illustrate the semblance property established in the preceding pages for shot-geophone migration. These examples expose the dramatic contrast between image (or common-image-point) gathers produced by shot-geophone migration and those produced by other forms of prestack depth migration. In all three examples, the formation of caustics leads to failure of the semblance principle for Kirchhoff (or Generalized Radon Transform) common scattering angle migration (Xu et al., 2001; Brandsberg-Dahl et al., 2003). In all three examples the DSR assumption is satisfied for the acquisition offsets considered For the shot-geophone migration we employ the double square root approach, using a generalized screen propagator (GSP) approximation of the square root operator (Le Rousseau and De Hoop, 2001). We form angle image gathers by Radon transform in offset and time, following (de Bruin et al., 1990; Prucha et al., 1999). Conversion of 'slope' to scattering angle follows the method described in (De Hoop et al., 2003, (88)-(89)).

Lens model

This example is used in (Stolk, 2002; Stolk and Symes, 2004) to show that common offset and Kirchhoff (or generalized Radon transform) common scattering-angle migration produce strong kinematic artifacts in strongly refracting velocity models. The velocity model lens embedded in a constant background. This model is strongly refracting through the formation of triplications in the rayfields. Below the lens, at a depth of 2 km, we placed a flat, horizontal reflector. We synthesized data using a (4, 10, 20, 40) Hz zero phase bandpass filter as (isotropic) source wavelet, and a finite difference scheme with adequate sampling. A typical shot gather over the lens (Figure 8, shot position indicated by a vertical arrow in Figure 6) shows a complex pattern of reflections from the flat reflector that have propagated through the lens.

We migrated the data with the above mentioned depth-extrapolation approach. Figure 7 shows the image, which clearly reproduces the reflector. An angle image gather (at horizontal location indicated by a vertical line in Figure ?? (left)) is shown in Figure 10; for comparison we show the Kirchhoff common scattering angle image gather in FIgure 9) at the same location (left) reproduced from (Stolk and Symes, 2004), each trace of which is obtained by Kirchhoff migration restricted to common angle. The Kirchhoff image gather is clearly contaminated by numerous energetic non-flat events, while the wave equation image gather is not. Artifacts in the Kirchhoff image gather must be non flat and can be removed by 'dip' filtering in depth and angle, but only if the velocity model is perfectly well known. In the wave equation image gather we observe a hint of residual moveout, which we attribute to reduced accuracy of the DSR propagator at large propagation angles. The image gathers have an increase in amplitude with increase in scattering angle in common.

Valhall lens model

This example is used in (Brandsberg-Dahl et al., 2003). The compressional-wave velocity model (Figure 11) is a simplication of the geological setting of the Valhall field. The model is in fact isotropic elastic, but the main heterogeneity appears in the compressional wave velocity. It consists of a slow Gaussian lens (gas); below the lens, at a depth of 1.5 km, we placed a reflector that is partly horizontal (a reservoir) and partly dipping to the left. One can view the dipping part of the reflector as a model fault plane. Above the reflector, the Gaussian lens is embedded in a constant gradient (0.45 s⁻¹) background; below the reflector the velocity is constant. Again, this model is strongly refracting.

We synthesized multi-component elastic-wave data using a bandpass filter with dominant frequency 35 Hz as (isotropic, explosive) source wavelet, and a finite difference scheme with close to adequate sampling. (Some numerical dispersion is present, but the sampling would have been unrealistically fine to remove all dispersive effects associated

with relatively low shear-wave velocities.) We extract the vertical component to suppress the shear-wave contributions. A typical shot gather over the lens (Figure 13, vertical component, shot position indicated by a vertical arrow in Figure 11) shows a complex pattern of reflections from the reflector propagated through the lens; we note the weak, remaining contributions from mode coverted waves at later times that will not be treated properly by our acoustic-wave migration scheme here.

We migrated the data with the above mentioned depth-extrapolation approach. Figure 12 shows the image. An angle image gather (at horizontal location indicated by a vertical line in Figure 11) is shown in Figure 14 (right); for comparison we show the angle image gather at the same location (left) reproduced from (Brandsberg-Dahl et al., 2003), which is obtained by generalized Radon transform migration (without focusing in dip or the application of isochron filters). The left image gather is, again, clearly contaminated by energetic non-flat events, while the right image gather is not.

Marmousi derived model

To establish the absence of artifacts in a geologically yet more realistic model, we adopt a model derived from the Marmousi model (Xu et al., 2001). It is based on a smoothing of the Marmousi velocity model and superimposing a layer of thickness 100 m and contrast 10 m/s at depth 2400 m (Figure 15 (top)). The smoothing was carried out with a low-pass filter, Gaussian shaped of half-power radius 150 m.

The data were generated, using an appropriately sampled finite difference scheme, as the difference between the data in the smooth, reference, model (without the layer) and the data in the model with the layer. The source was isotropic and dilational; the source wavelet was obtained as a (5, 13, 40, 55) Hz bandpass filter – with a time delay of 56 ms. Multi-pathing is prevalent in the right part of the model. A typical shot gather is shown in Figure 16 with shot position indicated by a vertical arrow in Figure 15 (top)); it shows, again, a very complex pattern of reflections.

We migrated the data with the above mentioned depth-extrapolation approach. Figure 15 (right) shows the image, in which the two reflectors are clearly resolved. An angle image gather (at horizontal location indicated by a vertical line in Figure 15 (top)) is shown in Figure 17 (right); for comparison we show the angle image gather at the same location (left) reproduced from (Stolk and Symes, 2004), each trace of which is obtained by Kirchhoff migration restricted to common scattering angle. The left image gather is, again, contaminated by energetic non-flat events; one artifact is indicated by a curve. The right image gather does not contain artifacts, as expected.

CONCLUSION

We have demonstrated, mathematically and by example, that shot-geophone migration produces artifact-free image volumes, assuming (i) kinematically correct and relatively smooth velocity model, (ii) incident energy traveling downwards, reflected energy traveling upwards, and (iii) enough data to uniquely determine rays corresponding to events in the data. The examples compared shot-geophone migration with Kirchhoff common scattering angle migration. While the latter technique bins data only implicitly, it is like other binwise migration schemes, such as common offset migration, in generating kinematic image artifacts in prestack data when the velocity model is sufficiently complex to strongly refract waves.

The recent literature contains a number of comparisons of Kirchhoff and wave equation migration (for example, (Albertin et al., 2002; Fliedner et al., 2002)). Performance differences identified in these reports have been ascribed to a wide variety of factors, such as differences in anti-aliasing and decimation strategies, choice of time fields used in Kirchhoff imaging, and "fidelity" to the wave equation. These factors surely affect performance, but reflect mainly implementation decisions. The difference identified and demonstrated in this paper, on the other hand, is *fundamental*: it flows from the differing formulations of prestack imaging (and modeling) underlying the two classes of methods. No implementation variations can mask it.

In fact, we have shown that implementation has at most a secondary impact on kinematic accuracy of shot-geophone imaging. Its basic kinematics is shared not just by the two common depth extrapolation implementations - shot profile, double square root - but also by a variant of reverse time imaging and even by a Kirchhoff or Generalized Radon Transform operator of appropriate construction. Naturally these various options differ in numerous ways, in their demands on data quality and sampling and in their sensitivity to various types of numerical artifacts. However in the ideal limit of continuous data and discretization-free computation, all share an underlying kinematic structure and offer the potential of artifact-free data volumes when the assumptions of our theory are satisfied, even in the presence of strong refraction and multiple arrivals at reflecting horizons.

It remains to address three shortcomings of the theory. The first is its reliance on the "DSR" assumption, i.e. no turning rays. The numerical investigations of Biondi and Shan (2002) suggested that reverse time (two-way) wave equation migration, as presented here, could be modified by inclusion of nonhorizontal offsets to permit the use of turning energy, and indeed to image reflectors of arbitrary dip. This latter possibility has been understood in the context of (stacked) images for some time (Yoon et al., 2003). Biondi and Shan (2002) present prestack image gathers for horizontal and vertical offsets which suggest that a similar flexibility may be available for the shot-geophone extension. Biondi and Symes (2004) give a local analysis of shot-geophone image formation using nonhorizontal

offsets, whereas Symes (2002) studied globally the formation of kinematic artifacts in a horizontal / vertical offset image volume. In contrast to the horizontal offset / DSR setting, such artifacts in general offset shot-geophone image volumes cannot be entirely ruled out. However kinematic artifacts cannot occur at arbitrarily small offset, in contrast to the formation of artifacts at all offsets in binwise migration.

A second limitation of our main result is its assumption that ray kinematics are completely determined by the data. Of course this is no limitation for the 2D synthetic examples presented above. "True 3D" acquisition is not unknown (Brandsberg-Dahl et al., 2003), but is uncommon - most contemporary data is acquired with narrow-azimuth streamer equipment. For such data, we cannot in general rule out the appearance of artifacts due to multiple ray pairs satisfying the shot-geophone kinematic imaging conditions. However two observations suggest that all is not lost. First, for ideal "2.5D" structure (independent of crossline coordinate) and perfect linear survey geometry (no feathering), all energetic rays remain in the vertical planes through the sail line, and our analysis applies without alteration to guarantee imaging fidelity. Second, the conditions that ensure absence of artifacts are open, i.e. small perturbations of velocity and source and receiver locations cannot affect the conclusion. Therefore shot-geophone imaging fidelity is robust against mild crossline heterogeneity and small amounts of cable feathering. Note that nothing about the formulation of our modeling or (adjoint) migration operators requires areal geometry - the operators are perfectly well-defined for narrow azimuth data.

A very intriguing and so far theoretically untouched area concerns the potential of *multiple* narrow azimuth surveys, with distinct central azimuths, to resolve the remaining ambiguities of single azimuth imaging.

A third, and much more fundamental, limitation pertains to migration itself. Migration operators are essentially adjoints to *linearized* modeling operators. The kinematic theory of migration requires that the velocity model be slowly varying on the wavelength scale, or at best be slowly varying except for a discrete set of fixed, regular interfaces. The most challenging contemporary imaging problems, for example subsalt prospect assessment, transgress this limitation, in many cases violently. Salt-sediment interfaces are amongst the unknowns, especially bottom salt, are quite irregular, and are perhaps not even truly interfaces. Very clever solutions have been and are being devised for these difficult imaging problems, but the theory lags far, far behind the practice.

Acknowledgements

This work was supported in part by National Science Foundation, and by the sponsors of The Rice Inversion Project (TRIP).

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APPENDIX A

In this appendix we establish the relation between the appearance of events in the data and the presence of reflectors in the migrated image. This relation is the *same* for the forward modeling operator and for its adjoint, the migration operator.

The reasoning presented here shares with (Stolk and De Hoop, 2001) the identification of events, respectively reflectors, by high frequency asymptotics in phase space, but differs in that it does not explicitly use oscillatory integral representations of F[v]. Instead, this argument follows the pattern of Rakesh's analysis of shot profile migration kinematics (Rakesh, 1988). It can be made mathematically rigorous, by means of the so-called Gabor calculus in the harmonic analysis of singularities (see (Duistermaat, 1973) Ch. 1).

Our analysis is based on the recognition that the shot-geophone predicted data field $u(\mathbf{x}_r, t; \mathbf{x}_s)$, defined by equation (6), is the value at $\bar{\mathbf{x}} = \mathbf{x}_r$ of the space-time field $u(\bar{\mathbf{x}}, t; \mathbf{x}_s)$, which solves

$$\frac{1}{v^2(\bar{\mathbf{x}})} \frac{\partial^2 u}{\partial t^2} (\bar{\mathbf{x}}, t; \mathbf{x}_s) - \nabla_{\bar{\mathbf{x}}}^2 u(\bar{\mathbf{x}}, t; \mathbf{x}_s) = \int dh \, R(\bar{\mathbf{x}} - \mathbf{h}, \mathbf{h}) \frac{\partial^2}{\partial t^2} G(\bar{\mathbf{x}} - 2\mathbf{h}, t; \mathbf{x}_s)$$
(46)

This equation follows directly by applying the wave operator to both sides of equation (6).

The appearance of an event at a point $(\mathbf{x}_s, \mathbf{x}_r, t_{sr})$ in the data volume is equivalent to the presence of a sizeable Fourier coefficient for a plane wave component

$$e^{i\omega(t-\mathbf{p}_s\cdot\bar{\mathbf{x}}_s-\mathbf{p}_r\cdot\bar{\mathbf{x}}_r)}$$

in the acoustic field for frequencies ω within the bandwidth of the data, even after muting out all events at a small distance from $(\mathbf{x}_s, \mathbf{x}_r, t_{sr})$.

Note that the data does not necessarily fully determine this plane wave component, i.e. the full 3D event slownesses \mathbf{p}_s , \mathbf{p}_r . In this appendix, \mathbf{p}_s , \mathbf{p}_r are assumed to be compatible with the data, in the sense just explained.

Assume that these frequencies are high enough relative to the length scales in the velocity that such local plane wave components propagate according to geometric acoustics. This assumption tacitly underlies much of reflection processing, and in particular is vital to the success of migration.

That is, solutions of wave equations such as (46) carry energy in local plane wave components along rays. Let $(\mathbf{X}_r(t), \mathbf{P}_r(t))$ denote such a ray, so that $\mathbf{X}_r(t_{sr}) = \mathbf{x}_r, \mathbf{P}_r(t_{sr}) = \mathbf{p}_r$. Then at some point the ray must pass through a point in phase space at which the source term (right hand side) of equation (46) has significant energy - otherwise the ray would never pick up any energy at all, and there would be no event at time t_{sr} , receiver position \mathbf{x}_r , and receiver slowness \mathbf{p}_r . [Supplemented with proper mathematical boiler-plate, this statement is the celebrated *Propagation of Singularities* theorem of Hörmander, (Hormander, 1983; Taylor, 1981).]

The source term involves (i) a product, and (ii) an integral in some of the variables. The Green's function $G(\bar{\mathbf{x}}_s, t, \mathbf{x}_s)$ has high frequency components along rays from the source, i.e. at points of the form $(\mathbf{X}_s(t_s), \mathbf{P}_s(t_s))$ where $\mathbf{X}_s(0) = \mathbf{x}_s$ and $t_s \geq 0$. [Of course this is just another instance of Propagation of Singularities, as the source term in the wave equation for $G(\bar{\mathbf{x}}_s, t_s, \mathbf{x}_s)$ is singular only at $(\mathbf{x}_s, 0)$.] That is, viewed as a function of $\bar{\mathbf{x}}_s$ and t_s , $G(\cdot, \cdot; \mathbf{x}_s)$ will have significant Fourier coefficients for plane waves

$$e^{i\omega(\mathbf{P}_s(t_s)\cdot\bar{\mathbf{x}}_s+t_s)}$$

We characterize reflectors in the same way: that is, there is a (double) reflector at $(\bar{\mathbf{x}}_s, \bar{\mathbf{x}}_r)$ if \bar{R} has significant Fourier coefficients of a plane wave

$$e^{i(\mathbf{k}_s \cdot \bar{\mathbf{x}}_s' + \mathbf{k}_r \cdot \bar{\mathbf{x}}_r')}$$

for some pair of wavenumbers \mathbf{k}_s , \mathbf{k}_r , and for generic points $(\bar{\mathbf{x}}_s', \bar{\mathbf{x}}_r')$ near $(\bar{\mathbf{x}}_s, \bar{\mathbf{x}}_r)$. Presumably then the product $R(\bar{\mathbf{x}}_s', \mathbf{x})G(\bar{\mathbf{x}}_s', t_s; \mathbf{x}_s)$ has a significant coefficient of the plane wave component

$$e^{i((\mathbf{k}_s + \omega \mathbf{P}_s(t_s)) \cdot \bar{\mathbf{x}}_s' + \mathbf{k}_r \cdot \mathbf{x} + \omega t_s)}$$

for $\bar{\mathbf{x}}'_s$ near $\bar{\mathbf{x}}_s$, \mathbf{x} near $\bar{\mathbf{x}}_r$; note that implicitly we have assumed that $\bar{\mathbf{x}}_s$ (the argument of G) is located on a ray from the source with time t_s . The right-hand side of equation (46) integrates this product over $\bar{\mathbf{x}}_s$. This integral will be negligible unless the phase in $\bar{\mathbf{x}}_s$ is

stationary: that is, to produce a substantial contribution to the RHS of equation (46), it is necessary that

$$\bar{\mathbf{x}}_s = \mathbf{X}_s(t_s), \ \mathbf{k}_s + \omega \mathbf{P}_s(t_s) = 0 \tag{47}$$

Supposing that this is so, the remaining exponential suggests that the RHS of equation (46) has a sizeable passband component of the form

$$e^{i(\mathbf{k}_r \cdot \mathbf{x} + \omega t_s)}$$

for \mathbf{x} near $\bar{\mathbf{x}}_r$. As was argued above, this RHS will give rise to a significant plane wave component in the solution u arriving at \mathbf{x}_r at time $t_{sr} = t_s + t_r$ exactly when a ray arriving at \mathbf{x}_r at time t_{sr} starts from a position in space-time with the location and wavenumber of this plane wave, at time $t_s = t_{sr} - t_r$: that is,

$$\mathbf{X}_r(t_s) = \bar{\mathbf{x}}_r, \ \omega \mathbf{P}_r(t_s) = \mathbf{k}_r \tag{48}$$

We end this appendix with a remark about the case of *complete coverage*, i.e. sources and receivers densely sample a fully 2D area on or near the surface. Assuming that the effect of the free surface has been removed, so that all events may be viewed as samplings of an upcoming wavefield, the data (2D) event slowness uniquely determines the wavefield (3D) slowness through the eikonal equation. Thus an event in the data is characterized by its (3D) moveout: locally, by a moveout equation $t = T(\mathbf{x}_s, \mathbf{x}_r)$, and infinitesimally by the source and receiver slownesses

$$\mathbf{p}_s = \nabla_{\mathbf{x}_s} T, \ \mathbf{p}_r = \nabla_{\mathbf{x}_r} T$$

In this case, the data event uniquely determines the source and receiver rays.

APPENDIX B

This appendix gives a quick derivation of equations (17), (18), and (39), which give prescriptions for computing the adjoints of the horizontal-offset shot-geophone modeling operator and of its double square root approximation, respectively. These are examples of the *adjoint state* method for computing the adjoints of operators defined by simulations. Tarantola (1987) gives more examples of this type of computation.

Defining the adjoint implies specifying an innter product on both the input and output spaces of the operator. The computation given here presumes the standard (" L^2 ") inner product for both, given by

$$\langle f, g \rangle = \int \bar{f}g,$$

where the integration takes place over all variables on which the functions f, g depend, and the complex conjugation is included to permit complex valued functions when necessary.

Reverse time shot-geophone migration with horizontal offsets

Recall that the horizontal offset shot-geophone modeling operator is defined by

$$\bar{F}_z[v]\bar{R}_z(\mathbf{x}_r, t; \mathbf{x}_s) = u(\mathbf{x}_r, t; \mathbf{x}_s),$$

where u solves the inhomogeneous wave equation

$$\left(\frac{1}{v^2(\bar{\mathbf{x}}_r)}\frac{\partial^2}{\partial t^2} - \nabla_{\bar{\mathbf{x}}_r}^2\right) u(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) = w_s(\bar{\mathbf{x}}_r, t; \mathbf{x}_s), \tag{49}$$

and

$$w_s(\bar{\mathbf{x}}_r, t; \mathbf{x}_s) = \int d\bar{x}_s \int d\bar{y}_s \bar{R}_z \left(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \frac{\bar{z}_r + \bar{z}_s}{2}\right) \delta(\bar{z}_r - \bar{z}_s) \frac{\partial^2}{\partial t^2} G(\bar{\mathbf{x}}_s, t; \mathbf{x}_s). \tag{50}$$

According to the standard definition, the adjoint $F_z[v]^*$ must satisfy for all possible data d and horizontal offset reflectivity \bar{R}_z

$$\langle \bar{F}_{z}[v]^{*}d, \bar{R}_{z} \rangle = \langle d, \bar{F}[v]\bar{R}_{z} \rangle = \int \int dx_{s} dx_{r} \int_{0}^{T} dt \, d(\mathbf{x}_{r}, t; \mathbf{x}_{s}) u(\mathbf{x}_{r}, t; \mathbf{x}_{s})$$

$$= \int dx_{s} \int dx \int_{0}^{T} dt \, \left\{ \int dx_{r} \, d(\mathbf{x}_{r}, t; \mathbf{x}_{s}) \delta(\mathbf{x} - \mathbf{x}_{r}) \right\} u(\mathbf{x}, t; \mathbf{x}_{s}),$$

$$= \int dx_{s} \int dx \int_{0}^{T} dt \, \left[\left(\frac{1}{v^{2}} \frac{\partial^{2}}{\partial t^{2}} - \nabla^{2} \right) u^{*}(\mathbf{x}, t; \mathbf{x}_{s}) \right] u(\mathbf{x}, t; \mathbf{x}_{s}), \tag{51}$$

provided that the adjoint field u^* satisfies

$$\left(\frac{1}{v(\mathbf{x})^2}\frac{\partial^2}{\partial t^2} - \nabla^2\right)u^*(\mathbf{x}, t; \mathbf{x}_s) = \int d\mathbf{x} d(\mathbf{x}_r, t; \mathbf{x}_s)\delta(\mathbf{x}_r - \mathbf{x}),\tag{52}$$

and $u^* \equiv 0, t >> 0, z > 0$. Notice that equation (52) is identical to equation (18).

Integration by parts on the right hand side of equation (51) shows that

$$\langle d, \bar{F}[v]\bar{R}_z \rangle = \int dx_s \int dx \int_0^T dt \left[\left(\frac{1}{v^2} \frac{\partial^2}{\partial t^2} - \nabla^2 \right) u(\mathbf{x}, t; \mathbf{x}_s) \right] u^*(\mathbf{x}, t; \mathbf{x}_s)$$

(boundary terms in integration by parts vanish because (i) $u \equiv 0, t << 0$; (ii) $u^* \equiv 0, t >> 0$; (iii) both vanish for large \mathbf{x} , at each t)

$$= \int dx_s \int d\mathbf{x} \int_0^T dt \, w_s(\mathbf{x}, t; \mathbf{x}_s) u^*(\mathbf{x}, t; \mathbf{x}_s).$$

Referring to the definition (50) of w_s , one sees that this integral is

$$= \langle \bar{R}_z, \bar{F}_z[v]^* d \rangle,$$

when $\bar{F}_z[v]^*$ is given by equation (17).

Double square root migration

As explained above, computing the adjoint of the double square root modeling operator (defined in equation (36)) boils down to computing the adjoint of the operator $H: f \mapsto u|_{z=0}$ where f and u are linked by

$$\frac{\partial}{\partial \bar{z}}u(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t) = B_{\text{DSR}}u(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t) + f(\bar{x}_r, \bar{x}_s, \bar{y}_r, \bar{y}_s, \bar{z}, t), \ u \equiv 0, \ z >> 0,$$
(53)

in which B_{DSR} is the double square root operator,

$$B_{\rm DSR} = -i \left(\sqrt{-v^{-2}(\bar{\mathbf{x}}_r) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_r, \bar{y}_r}^2} + \sqrt{-v^{-2}(\bar{\mathbf{x}}_s) \frac{\partial^2}{\partial t^2} + \nabla_{\bar{x}_s, \bar{y}_s}^2} \right).$$

Let $d(x_r, x_s, y_r, y_s, t)$ be a data-like field, and observe that

$$\langle d, Hf \rangle = \int dx_r \int dx_s \int dy_r \int dy_s \int dt \, d(x_r, x_s, y_r, y_s, t) u(x_r, x_s, y_r, y_s, 0, t)$$

$$= \int dx_r \int dx_s \int dy_r \int dy_s \int dz \int dt \, (d(x_r, x_s, y_r, y_s, t) \delta(z)) u(x_r, x_s, y_r, y_s, z, t)$$

$$= \int dx_r \int dx_s \int dy_r \int dy_s \int dz \int dt \, \left[\left(-\frac{\partial u^*}{\partial z} + B_{\text{DSR}} u^* \right) u \right] (x_r, x_s, y_r, y_s, z, t),$$

provided that u^* solves

$$\left(-\frac{\partial u^*}{\partial z} + B_{\text{DSR}}u^*\right)(x_r, x_s, y_r, y_s, z, t) = d(x_r, x_s, y_r, y_s, t)\delta(z), \ u^* \equiv 0, \ z << 0.$$

Because the single square root operators are skew-adjoint, so is the operator B_{DSR} is skew-adjoint: its adjoint (with respect to the Hermitian L^2 inner product) is its negative. Integrating by parts in z, one obtains

$$\langle d, Hf \rangle =$$

$$= \int dx_r \int dx_s \int dy_r \int dy_s \int dz \int dt \left[u^* \left(\frac{\partial u}{\partial z} - B_{DSR} u \right) \right] (x_r, x_s, y_r, y_s, z, t)$$

$$= \langle u^*, f \rangle,$$

whence $H^*d = u^*$, as claimed in equation (39).

APPENDIX C

The square root

$$-\mathrm{i}\sqrt{-v^{-2}(x,y)\frac{\partial^2}{\partial t^2} + \nabla_{x,y}^2},$$

is (relatively) easy to understand as an operator via the Fourier transform, if the velocity field v is laterally homogeneous (constant in x, y - we suppress for the moment the depenence of v on z). A different approach is required if v is laterally heterogeneous, certainly the case of interest in our work. The theory of pseudodifferential operators gives a framework within which to understand and even compute with such expressions. This formidable-sounding phrase connotes a quite simple and natural idea: if the variation of v is slow on the scale of a wavelength, then to good approximation the wave will see a locally constant velocity. So it should still be possible to define the action of this operator through the Fourier transform. The words "slow" and "approximation" hint that a logically consistent realization of this idea must be a variant of high frequency asymptotics, and that is the case. A good account of the general theory is Taylor's book (Taylor, 1981). This appendix presents a very skeletal treatment of the square root operator from this point of view. For careful application of the theory to one-way wave propagation, see (Stolk, 2004).

In order to stay close to the intended application, we use ω , k_x , k_y as Fourier variables, despite some resulting awkwardness in notation. A pseudodifferential operator is one that can be represented as an oscillatory integral of the type

$$Au(x,y,t) = \int dk_x \int dk_y \int d\omega a(x,y,t,k_x,k_y,\omega) e^{i(k_x x + k_y y + \omega t)} \hat{u}(k_x,k_y,\omega), \tag{54}$$

in which \hat{u} denotes the Fourier transform of u.

The kernel a(...) is called the *symbol* of the operator. Symbols are not permitted to be arbitrary functions in this theory, but must obey various restrictions. The (sub)class of operators of interest to us are defined by symbols which have these properties:

• polynomial growth at infinity in the Fourier variables:

$$a(x, y, t, k_x, k_y, \omega) = O((k_x^2 + k_y^2 + \omega^2)^{\frac{m}{2}}),$$

in which m is the *order* of the operator, which may be fractional.

• a is infinitely often differentiable in all of its variables, and the derivatives are symbols of the same class; each partial derivative in the Fourier variables lowers the order by one;

• a has an asymptotic expansion

$$a(x, y, t, k_x, k_y, \omega) \sim \sum_{j=0}^{\infty} a_{m-j}(x, y, t, k_x, k_y, \omega),$$

with each term a_j homogeneous in the Fourier variables of degree j. The expansion is asymptotic, in the sense that truncating it at j leaves a difference between left and right sides which is of order m - j - 1 in the Fourier variables. The leading order term a_m is homogeneous of order m and is called the *principal symbol* of the operator.

Note that the theory is not at all restricted to three space-time variables, but can accommodate any number of independent variables of any (or no) physical significance. Also the class of symbols defined by the above requirements is fairly special; see Tayler (1981) for a description of much more general classes of symbols and insight into the role of this special but important subclass.

The horizontal wave operator can be represented as such an oscillatory integral, via the basic properties of the Fourier transform:

$$\left(-v^{-2}(x,y)\frac{\partial^2}{\partial t^2} + \nabla_{x,y}^2\right)u(x,y,t) =$$

$$\frac{1}{(2\pi)^3} \int dk_x \int dk_y \int d\omega (v^2(x,y)\omega^2 - k_x^2 - k_y^2)e^{i(k_x x + k_y y + \omega t)}\hat{u}(k_x,k_y,\omega).$$

Note that in this case the symbol is a homogenous function of the Fourier variables of degree 2, so satisfies all of the conditions stated above (provided that the velocity is a smooth positive function, which we assume). The order is 2, which is consistent with the usual notion of order for the wave operator.

It is natural to think that the square root of the horizontal wave operator would be represented by the same sort of oscillatory integral, say B, with symbol equal to the square root of the wave operator's symbol. This is precisely correct for constant v. The theory of pseudodifferential operators shows that it is also true for (smoothly varying) nonconstant v, to leading order in the Fourier variables:

$$Bu(x,y,t) \equiv \int dk_x \int dk_y \int d\omega b(x,y,t,k_x,k_y,\omega) e^{i(k_x x + k_y y + \omega t)} \hat{u}(k_x,k_y,\omega)$$
 (55)

satisfies

$$B^{2}u(x,y,t) = B(Bu)(x,y,t) = \left(-v^{-2}(x,y)\frac{\partial^{2}}{\partial t^{2}} + \nabla_{x,y}^{2}\right)u(x,y,t)$$

The symbol b is of order 1,

$$b \sim b_1 + b_0 + b_{-1} + \dots$$

and

$$b_1(x, y, t, k_x, k_y, \omega) = (2\pi)^{-\frac{3}{2}} \operatorname{sgn}\omega \sqrt{v^{-2}(x, y)\omega^2 - k_x^2 - k_y^2}$$
$$= (2\pi)^{-\frac{3}{2}}\omega \sqrt{v^{-2}(x, y) - \omega^{-2}(k_x^2 + k_y^2)}.$$

A standard recursion computes the remaining terms $b_0, b_{-1}, ...,$ which do not in general vanish - see (Taylor, 1981), Lemma 6.2, p. 50 for a similar computation.

Clearly this construction fails at points in phase space where $|\omega| = v(x,y)\sqrt{k_x^2 + k_y^2}$, as the square root becomes singular there so cannot define a principal symbol. Physically, this condition marks the onset of nonpropagating or evanescent waves. See (Stolk, 2004) for a careful treatment of this problem. A resolution does not obviate the construction presented here, but merely requires that the symbol construction be modified near the singularity in the square root.

A crude approximation to the careful fix presented in (Stolk, 2004) is to restrict the integration in equation (55) to the region defined by $|\omega| > (1+\epsilon)v(x,y)\sqrt{k_x^2+k_y^2}$ for some choice of $\epsilon > 0$. This approximation will suffice for the remainder of the discussion. Its meaning: the operator defined by this limited range of integration will approximate the square root, i.e. its square will approximate the action of the horizontal wave operator, for functions whose localized Fourier transforms have significant high frequency energy only at (k_x, k_y, ω) satisfying the constraints. Localized Fourier transform means: multiply by a function vanishing outside of a small region, then Fourier transform. The notion of localized Fourier transform permits us to view the energy of a function as distributed in phase space - the position coordinates being the point of localization, the wavenumber coordinates being the Fourier variables used to describe the transform of the localized function. The uncertainty principle limits the precision with which we can associate energy to points in phase space.

Note that the b_1 is real and odd in the Fourier variables; the other terms in the asymptotic expansion inherit these properties also, and so to all finite orders in frequency is the total symbol b. It follows that -iB is real, i.e. maps real-valued functions to real valued functions. Indeed,

$$\overline{(-iBu(x,y,t))} = i \int dk_x \int dk_y \int d\omega b(x,y,t,k_x,k_y,\omega) e^{-i(k_xx+k_yy+\omega t} \hat{u}(k_x,k_y,\omega)$$

$$= i \int dk_x \int dk_y \int d\omega b(x,y,t,-k_x,-k_y,-\omega) e^{i(k_xx+k_yy+\omega t} \hat{u}(-k_x,-k_y,-\omega).$$

in which the last step results from the changes of variable $k_x \to -k_x, k_y \to -k_y, \omega \to -\omega$. Since u is real, $\bar{u}(-k_x, -k_y, -\omega) = \hat{u}(k_x, k_y, \omega)$. Since b is odd in the Fourier variables,

$$\overline{(-iBu(x,y,t))} = -i\int dk_x \int dk_y \int d\omega b(x,y,t,k_x,k_y,\omega) e^{i(k_xx+k_yy+\omega t)} \hat{u}(k_x,k_y,\omega)$$

$$=-iBu(x,y,t).$$

That is, -iBu is real-valued if u is real-valued, as was to be shown.

We can now derive the square-root equation (36) satisfied by an upgoing solution of the wave equation (22). For the remainder of the discussion, we re-introduce the z dependence of the various fields. We need several more properties of pseudodifferential operators, the first two of which generalize well-known properties of differential operators:

- if A_i has order m_i (i.e. its symbol does), i = 1, 2 then A_1A_2 is also a pseudodifferential operator and has order $m_1 + m_2$;
- (scalar) pseudodifferential operators commute to highest order: in the notation of the previous bullet, $[A_1, A_2] \equiv A_1 A_2 A_2 A_1$ has order $m_1 + m_2 1$;
- For any such operator A of order m, there exists an operator A^{\dagger} of order -m for which $A^{\dagger}Au \simeq u$ when u has no significant high frequency energy at points in phase space where the symbol of A vanishes;
- pseudodifferential operators do not change the locations in phase space of high frequency components: if B is such an operator, and localized Fourier components of u vanish to arbitrarily high order near a given direction in wavenumber space, then Bu has the same behaviour (this is sometimes called the "microlocal" property of pseudodifferential operators).

A short computation shows that (B denoting again the square root operator as above)

$$\left(\frac{\partial}{\partial z} - iB\right) \left(\frac{\partial}{\partial z} + iB\right) + \left[\frac{\partial}{\partial z}, iB\right] = \frac{1}{v(\mathbf{x})^2} \frac{\partial^2}{\partial t^2} - \nabla^2$$

The symbol of the z partial derivative is $-ik_z$, whereas the symbol of -iB is $-i\omega(...)$ in which the elided term is real and positive. "Upgoing" means: for the Fourier transform localized near x, y, z, t, significant energy is found only at wavenumbers satisfying the dispersion relation of the wave equation with ω , k_z having the same sign. Thus the symbol of the first factor cannot vanish where u (or the second factor acting on u, according to the last bullet above) has significant high frequency components. Thus according to the third bullet above, the wave equation (22) implies the double square root equation (36) for the upcoming solution, in which

$$C_{-} = \left(\frac{\partial}{\partial z} - iB\right)^{\dagger} \left[\frac{\partial}{\partial z}, iB\right]$$

and

$$A_{-} = \left(\frac{\partial}{\partial z} - \mathrm{i}B\right)^{\dagger}$$

The first three bullets above imply that A_{-} has order -1, and C_{-} has order zero. Therefore the operator $-iB + C_{-}$ appearing in equation (36) has the same principal symbol as -iB. Arguing further along these lines, one sees that the operators C_{-} and A_{-} can be dropped as suggested above without changing the location or orientation of high frequency components in the solution.

Some technical difficulty arises from the fact that B is actually a family of pseudodifferential operators in x, y, t parametrized by z, which in general is not a pseudodifferential operator in x, y, z, t. See (Stolk, 2004) and references cited there.

APPENDIX D

An integral or "Kirchhoff" representation of the shot-geophone migration operator is also possible. We mention this here to emphasize that the computational representation of the shot-geophone migrated field is not the determinant of its favorable kinematic properties: the Kirchhoff representation described here is in principle kinematically equivalent to two-way reverse migration, and to shot profile and double square root migrations within their domains of validity.

Application of standard high frequency asymptotics and stationary phase arguments to the integral representation of the shot-geophone field (3) gives

$$F[v]R(\mathbf{x}_r, t; \mathbf{x}_s) = \frac{\partial^2}{\partial t^2} \sum_{i,j} \int \int dx \, dh \, A^{(i,j)}(\mathbf{x}, \mathbf{h}, \mathbf{x}_s, \mathbf{x}_r) \, \delta(t - T^{(i,j)}(\mathbf{x}, \mathbf{h}, \mathbf{x}_s, \mathbf{x}_r)) R(\mathbf{x}, \mathbf{h})$$
(56)

in which $T^{(i,j)}(\mathbf{x}, \mathbf{h}, \mathbf{x}_s, \mathbf{x}_r)$ is the sum of the *i*th branch of the (one-way) traveltime from the source point \mathbf{x}_s to the source-ray scattering point $\mathbf{x} - \mathbf{h}$, and the *j*th branch of the traveltime from the receiver-ray scattering point $\mathbf{x} + \mathbf{h}$ to the receiver point \mathbf{x}_r , and $A^{(i,j)}(...)$ is an amplitude involving spreading factors, velocity, etc. (Stolk and Symes, 2004). The Kirchhoff shot-geophone migration formula is then

$$F^*[v]d(\mathbf{x}, \mathbf{h}) \simeq \int \int dx_s dx_r \sum_{i,j} A^{(i,j)}(\mathbf{x}, \mathbf{h}, \mathbf{x}_s, \mathbf{x}_r) \frac{\partial^2 d}{\partial t^2}(\mathbf{x}_s, \mathbf{x}_r, T^{(i,j)}(\mathbf{x}, \mathbf{h}, \mathbf{x}_s, \mathbf{x}_r))$$
(57)

Stolk and De Hoop (2001) derived these formulas in a different way for the special case $h_3 = 0$, i.e. horizontal depth-offset.

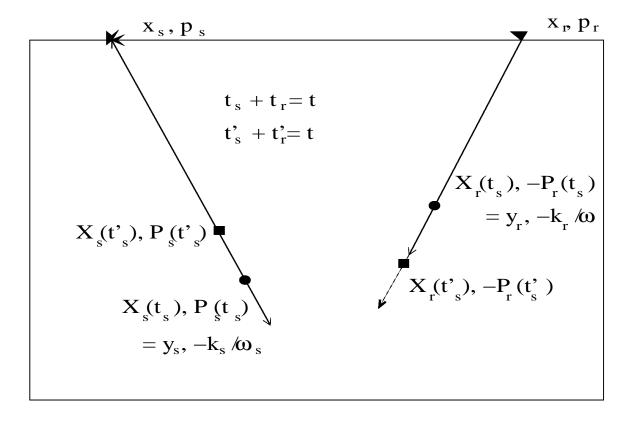


Fig. 1. Ray theoretic relation between data event and double reflector.

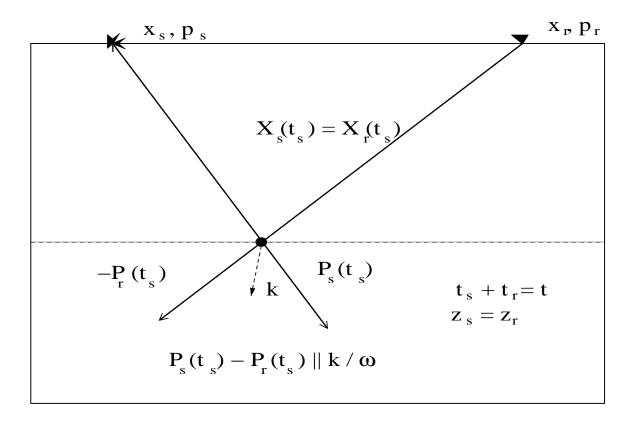


Fig. 2. Ray theoretic relation between data event and physical (single) reflector.

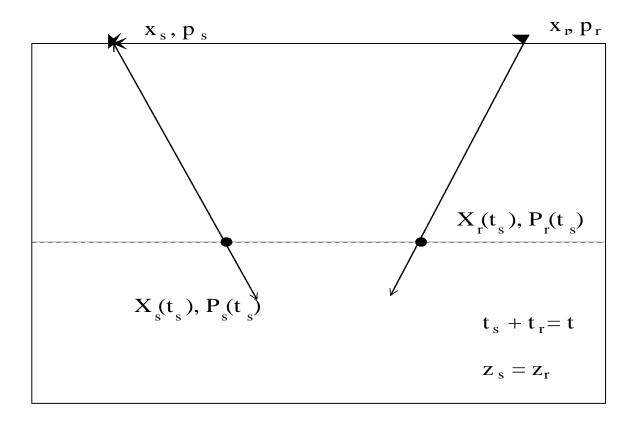


Fig. 3. Ray geometry for double reflector with horizontal offset only

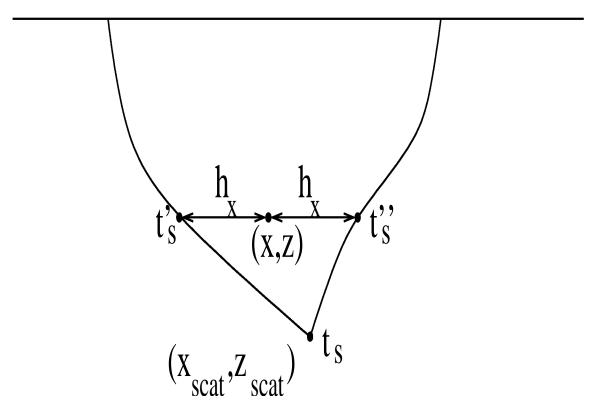


Fig. 4. Ray geometry for offset-time angle gather construction.

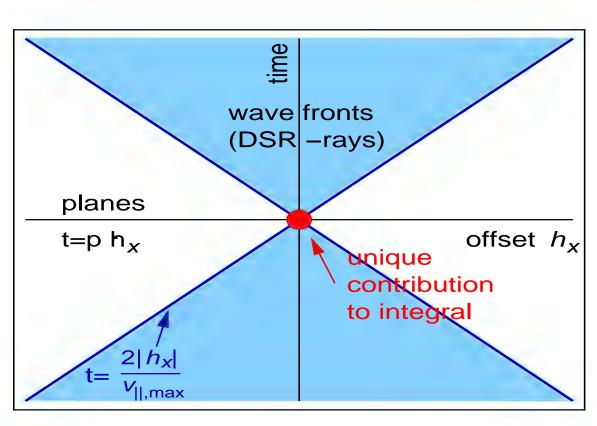


Fig. 5. Cone in phase space for energy admitted to angle gather construction.

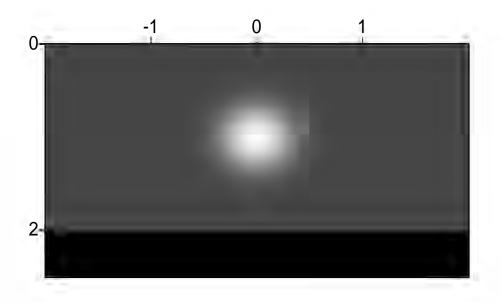


Fig. 6. Lens velocity model over flat reflector.

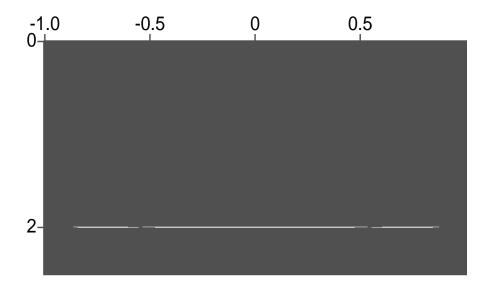


Fig. 7. DSR image of data lens velocity model, flat reflector.

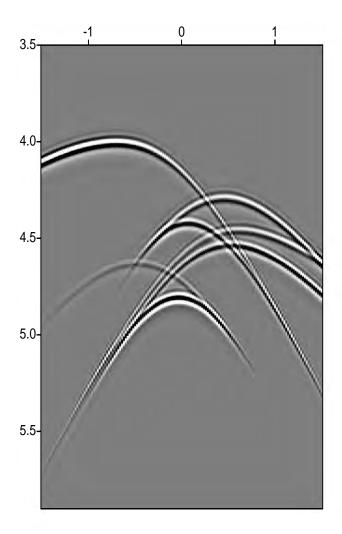


Fig. 8. Lens model, shot record at shot location -500 m.

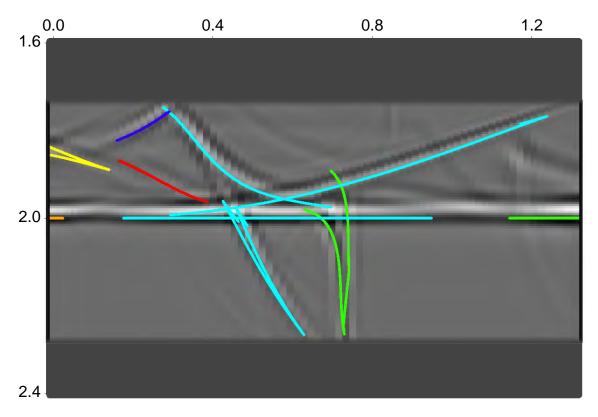


Fig. 9. Lens model, common image point gather obtained with the Kirchhoff angle transform at $x_m=300~\mathrm{m}.$

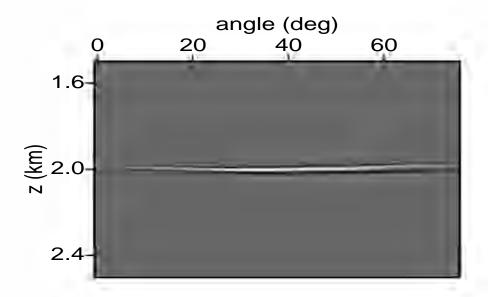


Fig. 10. Lens model, common image point gather obtained with the wave-equation angle transform (right) at $x_m=300$ m.

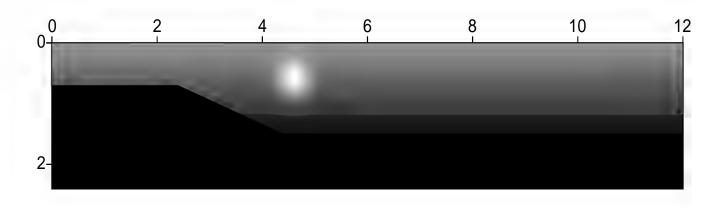


Fig. 11. Valhall velocity model.

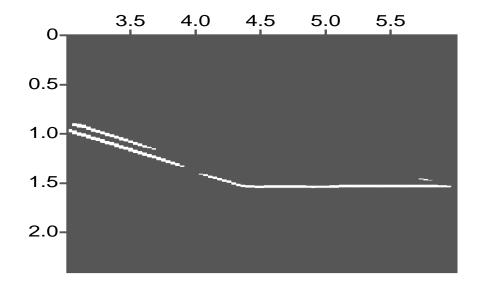


Fig. 12. Valhall DSR image.

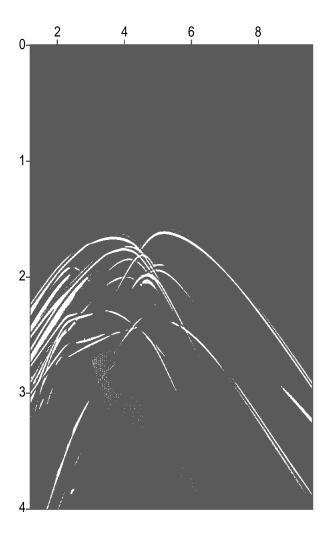
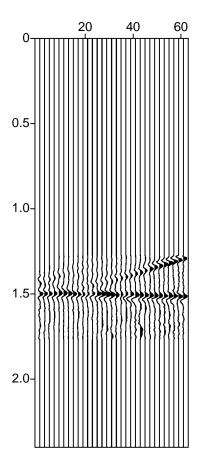


Fig. 13. Valhall lens model, shot record at shot location 4884 m.



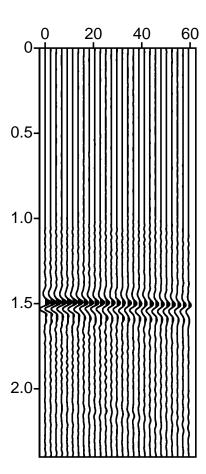


Fig. 14. Valhall lens model, common image point gathers obtained with the Kirchhoff angle transform (left) and the wave-equation angle transform (right) at 4680 m.

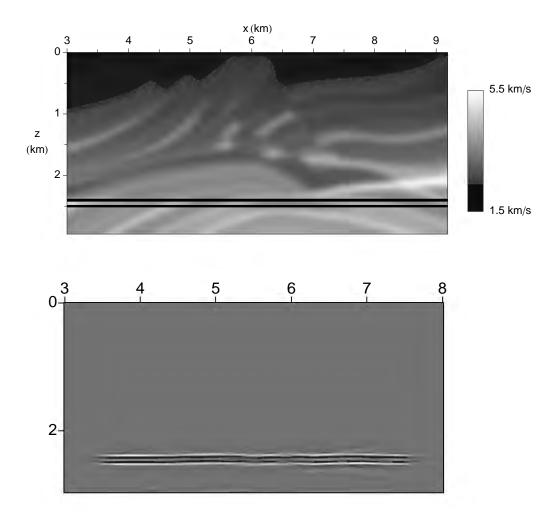


Fig. 15. Marmousi derived model (top) and DSR image (bottom).

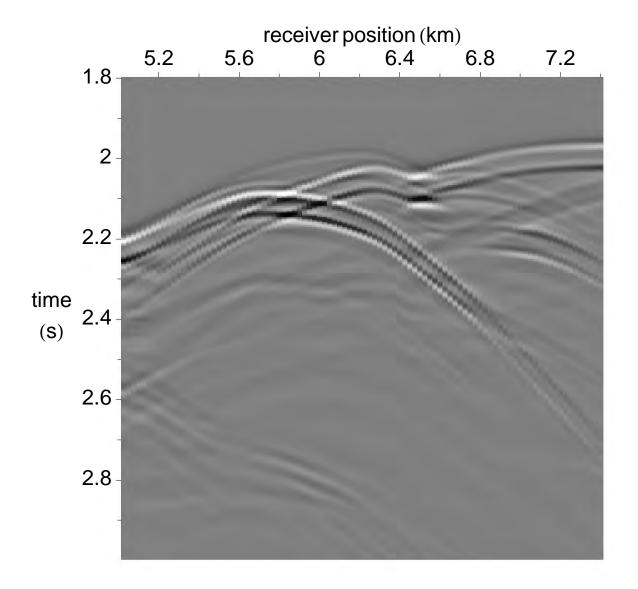


Fig. 16. Marmousi derived model, shot record at shot location 7500 m.

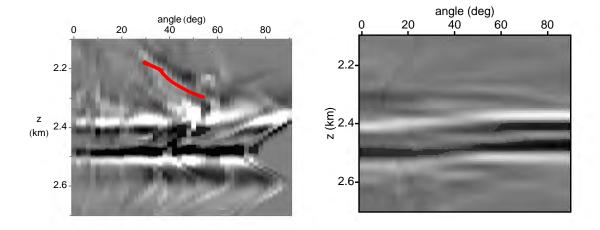


FIG. 17. Marmousi derived model, common image point gathers obtained with the Kirchhoff angle transform (left) and the wave-equation angle transform (right) at 6200 m.